

P1

Monday, March 15, 2021 4:33 PM

- Electromagnetic Waves (Plane Waves) -

We have the following equations from electrostatics:

$$1-) \nabla \times \vec{E} = 0$$

$$1-) \nabla \times \vec{B} = \mu_0 \vec{J}$$

$$2-) \nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$$

$$2-) \nabla \cdot \vec{B} = 0$$

Electrostatics

Magnetostatics

Re-arranging these equations (DC only)

$$1-) \nabla \times \vec{E} = 0$$

$$2-) \nabla \times \vec{B} = \mu_0 \vec{J}$$

$$3-) \nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$$

$$4-) \nabla \cdot \vec{B} = 0$$

Differential forms (point forms)

Integral forms

$$1-) \oint_C \vec{E} \cdot d\vec{l} = 0 \text{ (KVL)}$$

$$2-) \oint_C \vec{B} \cdot d\vec{l} = \mu_0 I \text{ (Ampere's law)}$$

$$3-) \int_S \vec{E} \cdot d\vec{s} = \frac{Q}{\epsilon_0} \text{ (Gauss law)}$$

$$4-) \int_S \vec{B} \cdot d\vec{s} = 0$$

Generalized forms: (AC + DC)

$$1-) \nabla \times \vec{E} = -\frac{d}{dt} \vec{B} \text{ (Faraday's law)}$$

$$2-) \nabla \times \vec{B} = \mu_0 \left( \vec{J} + \frac{d}{dt} \epsilon_0 \vec{E} \right) \text{ (Ampere's law)}$$

Maxwell's contribution.

$$3-) \nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$$

$$4-) \nabla \cdot \vec{B} = 0$$

Integral forms.

$$\oint_C \vec{E} \cdot d\vec{l} = V_{ind} = -\frac{d}{dt} \phi$$

$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 I + \frac{d}{dt} \mu_0 \epsilon_0 \int_S \vec{E} \cdot d\vec{s}$$

These 4 equations are called "Maxwell's equations", and they are all the equations necessary to solve any electromagnetic problem.

## Constitutive Parameters (Electrical properties of a medium)

1-) Permittivity =  $\epsilon$  = gives the amount of polarization.

If  $\epsilon$  is high, this means highly polarized medium.

For instance, water is such a medium. The  $\vec{E}$ -field is decreased inside such mediums.

$$\epsilon = \epsilon_0 \epsilon_r, \quad \epsilon_0 = 8.854 \times 10^{-12} \left(\frac{F}{m}\right), \quad \epsilon_r = \text{relative permittivity}$$

2-) Permeability =  $\mu$  = gives the amount of magnetization ( $e^-$  spin) of a matter. If  $\mu$  is high, more magnetization when inserted into a magnetic field. Fe is an example of highly magnetized material (Ferrites).

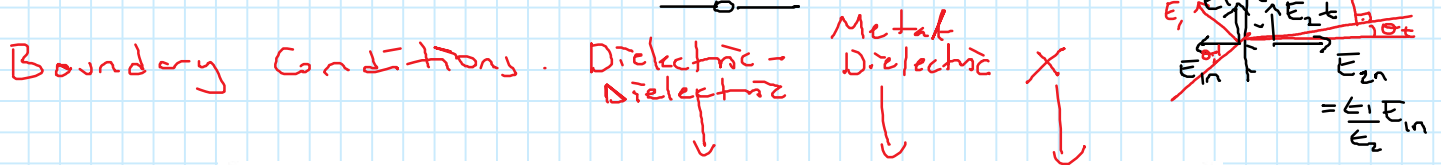
$$\mu = \mu_0 \mu_r, \quad \mu_0 = 4\pi \times 10^{-7} \left(\frac{H}{m}\right), \quad \mu_r = \text{relative permeability.}$$

3-) Conductivity =  $\sigma$  = gives how much current flows in the presence of  $\vec{E}$ -field in the medium.

$$\vec{J} = \sigma \vec{E} \quad (\text{Ohm's law in points form})$$

$\vec{J}$  ← Current density  $\left(\frac{A}{m^2}\right)$        $\vec{E}$  ← Electric field  $\left(\frac{V}{m}\right)$

If  $\sigma$  is high like in metals, then small  $\vec{E}$ -field can cause significant current.

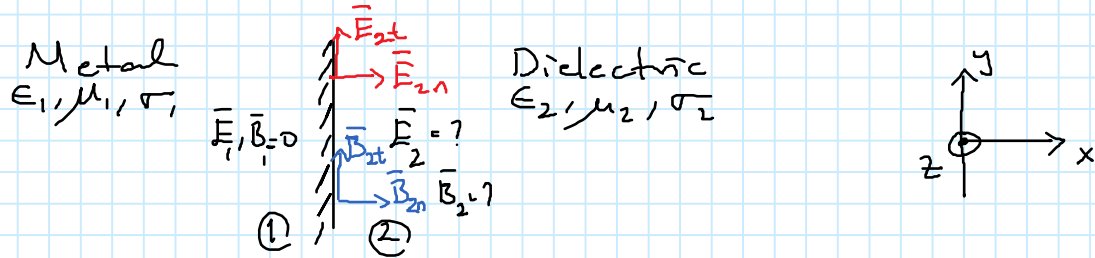


	General	Finite conductivity media, no sources or charges $\sigma_1, \sigma_2 \neq \infty$ $\mathcal{J}_s = 0; \mathcal{J}_{es} = 0$ $\mathcal{M}_s = 0; \mathcal{J}_{ms} = 0$	Medium 1 of infinite electric conductivity $(\mathcal{E}_1 = \mathcal{H}_1 = 0)$ $\sigma_1 = \infty; \sigma_2 \neq \infty$ $\mathcal{M}_s = 0; \mathcal{J}_{ms} = 0$	Medium 1 of infinite magnetic conductivity $(\mathcal{E}_1 = \mathcal{H}_1 = 0)$ $\mathcal{J}_s = 0; \mathcal{J}_{es} = 0$
Tangential electric field intensity	$-\hat{n} \times (\mathcal{E}_2 - \mathcal{E}_1) = \mathcal{M}_s$	$\hat{n} \times (\mathcal{E}_2 - \mathcal{E}_1) = 0$ $\hookrightarrow E_{2t} = E_{1t}$	$\hat{n} \times \mathcal{E}_2 = 0$	$-\hat{n} \times \mathcal{E}_2 = \mathcal{M}_s$
Tangential magnetic field intensity	$\hat{n} \times (\mathcal{H}_2 - \mathcal{H}_1) = \mathcal{J}_s$	$\hat{n} \times (\mathcal{H}_2 - \mathcal{H}_1) = 0$	$\hat{n} \times \mathcal{H}_2 = \mathcal{J}_s$	$\hat{n} \times \mathcal{H}_2 = 0$
Normal electric flux density	$\hat{n} \cdot (\mathcal{D}_2 - \mathcal{D}_1) = \mathcal{J}_{es}$	$\hat{n} \cdot (\mathcal{D}_2 - \mathcal{D}_1) = 0$ $\rightarrow D_{2n} = \epsilon_1 E_{1n}, \epsilon_2 E_{2n} = \epsilon_1 E_{1n}$	$\hat{n} \cdot \mathcal{D}_2 = \mathcal{J}_{es}$	$\hat{n} \cdot \mathcal{D}_2 = 0$
Normal magnetic flux density	$\hat{n} \cdot (\mathcal{B}_2 - \mathcal{B}_1) = \mathcal{J}_{ms}$	$\hat{n} \cdot (\mathcal{B}_2 - \mathcal{B}_1) = 0$	$\hat{n} \cdot \mathcal{B}_2 = 0$	$\hat{n} \cdot \mathcal{B}_2 = \mathcal{J}_{ms}$

This table gives us the relation between the fields ( $\vec{E}$  and  $\vec{B}$ ) at the boundary of two different mediums.

Ex'

Consider a metal to dielectric interface



Let us suppose that  $\vec{E}_1$  and  $\vec{B}_1$  at the boundary are known  
By using the table, we can obtain  $\vec{E}_2$  and  $\vec{B}_2$  at the boundary

Find  $\vec{E}_2$  and  $\vec{B}_2$

Ans

We can use the 2<sup>nd</sup> column in the table where medium 1 is the metal and medium 2 is the dielectric:

Inside metals:  $\vec{E} = 0 \Rightarrow \vec{E}_{1t} = \vec{E}_{1n} = 0$ ,  $B_{1t} = B_{1n} = 0$

→ Tangential  $\vec{E}$ -field:  $\hat{n} \times \vec{E}_{2t} = 0 \Rightarrow -\hat{a}_x \times \vec{E}_{2t} = 0 \Rightarrow \vec{E}_{2t} = 0$

→ Normal  $\vec{E}$ -field:  $\hat{n} \cdot \epsilon_2 \vec{E}_{2n} = \rho_s \left( \frac{C}{m^2} \right) \Rightarrow -\hat{a}_x \cdot \epsilon_2 \vec{E}_{2n} = \rho_s$

$$\Rightarrow -\hat{a}_x \cdot \epsilon_2 \hat{a}_x \vec{E}_{2n} = \rho_s$$

$$\Rightarrow \vec{E}_{2n} = \frac{\rho_s}{\epsilon_2} \left( \frac{V}{m} \right)$$

→ Tangential Mag Field:  $\hat{n} \times \vec{H}_2 = \vec{J}_s \Rightarrow \hat{a}_x \times \hat{a}_y \frac{B_{2t}}{\mu_2} = -\hat{a}_z J_s$

$$\Rightarrow B_{2t} = \mu_2 J_s \left( \frac{Vs}{m^2} \right)$$

→ Normal mag. field:  $\hat{n} \cdot \vec{B}_2 = 0 \Rightarrow B_{2n} = 0$

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# P4

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- In summary,  $\vec{E}$  and  $\vec{B}$  are zero inside metals.
- $\rho_s$  and  $\vec{J}_s = 0$  inside dielectrics and  $\sigma = 0$
- For metals,  $\sigma = \infty$ ,  $\rho_s$  and  $\vec{J}_s \neq 0$

## - Wave Equation -

Let us re-write Maxwell's equations.

Integral forms.

$$1-) \vec{\nabla} \times \vec{E} = -\frac{d}{dt} \vec{B} \quad (\text{Faraday's law}) \rightarrow \oint_C \vec{E} \cdot d\vec{l} = V_{ind} = -\frac{d}{dt} \phi$$

$$2-) \vec{\nabla} \times \vec{B} = \mu \vec{J} + \frac{d}{dt} (\mu \epsilon \vec{E}) \quad (\text{Ampere's law})$$

Maxwell's contribution.

$$\rightarrow \oint_C \vec{B} \cdot d\vec{l} = \mu I + \frac{d}{dt} \mu \oint_S \epsilon \vec{E} \cdot d\vec{s}$$

$$3-) \vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon} \rightarrow \oint_S \vec{E} \cdot d\vec{s} = \frac{Q}{\epsilon}$$

$$4-) \vec{\nabla} \cdot \vec{B} = 0 \rightarrow \oint_S \vec{B} \cdot d\vec{s} = 0$$

We can solve eqn. (1) and (2) simultaneously to get the wave equation (point forms)

Take the curl of 1<sup>st</sup> eqn:

$$\vec{\nabla} \times \vec{\nabla} \times \vec{E} = -\vec{\nabla} \times \frac{\partial \vec{B}}{\partial t} = -\frac{\partial}{\partial t} (\vec{\nabla} \times \vec{B})$$

Using the vector identity

$$\vec{\nabla} \times \vec{\nabla} \times \vec{A} = \nabla(\vec{\nabla} \cdot \vec{A}) - \nabla^2 \vec{A}$$

Then, we get

↳ Laplacian operator (2<sup>nd</sup> order space derivatives)

$$\vec{\nabla}(\vec{\nabla} \cdot \vec{E}) - \nabla^2 \vec{E} = -\frac{\partial}{\partial t} (\vec{\nabla} \times \vec{B})$$

Then,

$$\vec{\nabla} \times \vec{B} = \mu \vec{J} + \frac{\partial}{\partial t} \mu \epsilon \vec{E} \quad (2^{nd} \text{ eqn.})$$

$$\vec{\nabla}(\vec{\nabla} \cdot \vec{E}) - \nabla^2 \vec{E} = -\frac{\partial}{\partial t} \left( \mu \vec{J} + \frac{\partial}{\partial t} \mu \epsilon \vec{E} \right)$$

or

$$\underbrace{\vec{\nabla}(\vec{\nabla} \cdot \vec{E})}_{\frac{\rho}{\epsilon_0}} - \nabla^2 \vec{E} = -\frac{\partial}{\partial t} \mu \vec{J} - \frac{\partial^2}{\partial t^2} \mu \epsilon \vec{E}$$

$$\underbrace{\nabla(\nabla \cdot \vec{E})}_{\frac{\rho}{\epsilon}} - \nabla^2 \vec{E} = -\frac{\partial}{\partial t} \mu \vec{J} - \frac{\partial^2}{\partial t^2} \mu \epsilon \vec{E}$$

Also,  $\vec{J} = \sigma \vec{E}$

Then, we have

$$\frac{1}{\epsilon} (\nabla \cdot \rho) - \nabla^2 \vec{E} = -\frac{\partial}{\partial t} (\mu \sigma \vec{E}) - \frac{\partial^2}{\partial t^2} (\mu \epsilon \vec{E})$$

Re-arranging the terms:

$$\nabla^2 \vec{E} = \frac{1}{\epsilon} (\nabla \cdot \rho) + \mu \sigma \frac{\partial \vec{E}}{\partial t} + \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2} \quad (\text{Wave equation for } \vec{E}\text{-field})$$

We could do the same analysis for  $\vec{H}$ , we would have

$$\nabla^2 \vec{H} = \frac{1}{\mu} (\nabla \cdot \rho_m) + \mu \sigma_m \frac{\partial \vec{H}}{\partial t} + \mu \epsilon \frac{\partial^2 \vec{H}}{\partial t^2} \quad (\text{Wave eqn. for } \vec{H}\text{-field})$$

0 magnetic charge density = 0 (frictionless)  $\vec{B} = \mu \vec{H}$

Solution of these equations:

Let us use the wave eqn. for  $\vec{E}$ -field:

$$\nabla^2 \vec{E} = \frac{1}{\epsilon} (\nabla \cdot \rho) + \mu \sigma \frac{\partial \vec{E}}{\partial t} + \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2}$$

We want a solution in dielectric medium (air)

or

$$\rho = \vec{J} = 0 \quad \text{in } \vec{E}, \vec{H} \quad (\vec{E}(x,y,z), \vec{H}(x,y,z)) \longrightarrow z$$

In air (dielectric),  $\sigma = 0, \rho = \vec{J} = 0$

Wave Solution for Simple Medium (Source free and lossless) Simple media

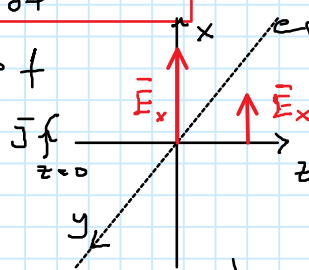
Then we obtain:

$$\nabla^2 \vec{E} - \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2} = 0 \quad (\text{Homogenous wave equation for simple medium})$$

Assume  $\vec{E} = \hat{a}_x E_x(z,t)$  type of solution. (plane wave)

$$\Rightarrow \nabla^2 \vec{E} = \hat{a}_x \frac{\partial^2 E_x(z,t)}{\partial z^2}$$

Substitute this into the wave equation



$$\hat{a}_x \frac{\partial^2 E_x(z, t)}{\partial z^2} - \mu \epsilon \hat{a}_x \frac{\partial^2 \bar{E}_x(z, t)}{\partial t^2} = 0$$

Initial conditions = Boundary conditions.

$$1-) E_x(0) = E_0$$

$$2-) E_x\left(\frac{2\pi}{k}\right) = E_0 \quad (\text{period } \lambda) \quad k = \omega \sqrt{\mu \epsilon}, \quad \omega = \text{radial frequency.}$$

The solution of this linear 2<sup>nd</sup> order homogenous differential equation is:

$$E_x(z, t) = E_0 \cos(\omega t - kz)$$

(Wave solution)

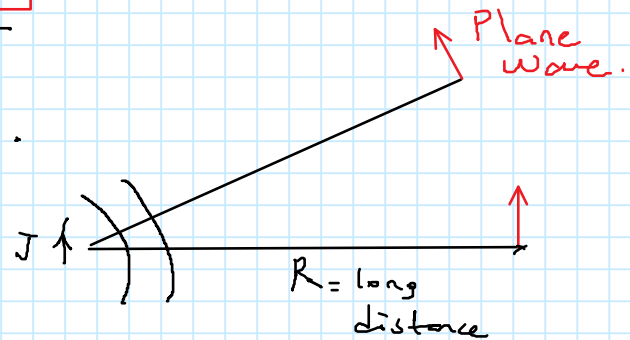
, where  $k$  = wave number

2 important remarks:

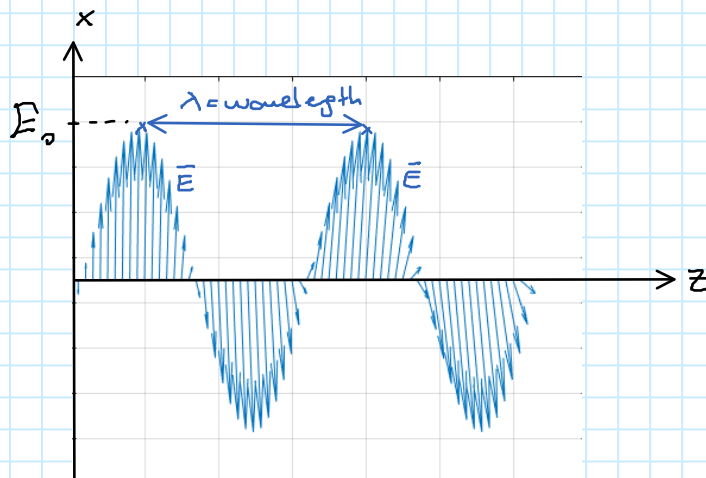
1-) At its origin,  $\bar{J}$  causes  $\bar{E}$  and  $\bar{H}$ .

2-) Assumption on the solution

$$\bar{E} = \hat{a}_x E_x(z, t)$$



Solution:



Phase Velocity:

Consider the plane wave solution

$$E_x(z, t) = E_0 \cos(\omega t - kz) \quad \left(\frac{v}{m}\right)$$

To find phase velocity

$$\omega t - kz = C_0 = \text{constant}$$

Take the derivative of both sides wrt.  $t$ .

$$\Rightarrow \frac{d}{dt}(\omega t) - k \frac{dz}{dt} = \frac{d}{dt} C_0$$

$$\omega - k \cdot v_p = 0$$

$$\Rightarrow v_p = \frac{\omega}{k} = \frac{\omega}{\omega \sqrt{\mu \epsilon}} = \frac{1}{\sqrt{\mu \epsilon}}$$

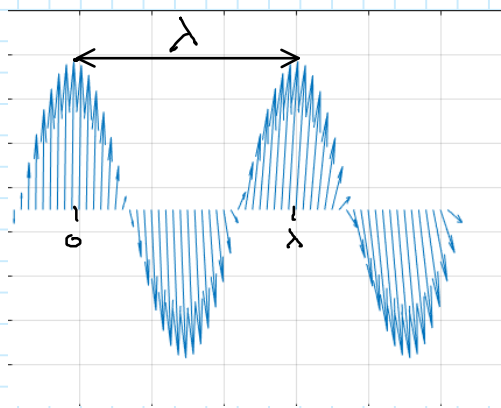
For air,  $v_p = c = \frac{1}{\sqrt{\mu_0 \epsilon_0}} = 3 \times 10^8 \text{ m/s}$ . (speed of light.)

$$v_p \Big|_{\text{water}} = \frac{1}{\sqrt{\mu_0 \epsilon_r \epsilon_0}} = \frac{1}{\sqrt{\epsilon_r} \sqrt{\mu_0 \epsilon_0}} = \frac{1}{\sqrt{\epsilon_r}} \times 3 \times 10^8 \text{ m/s}$$

Wavelength:

Consider the plane wave solution

$$E_x(z, t) = E_0 \cos(\omega t - kz) \quad \left(\frac{V}{m}\right)$$



At  $z=0$ : ( $t=0$ )

$$\omega t - kz = 0$$

$$0 = kz \Rightarrow z=0$$

At  $z=\lambda$ : ( $t=T$ )

$$\omega t = k\lambda$$

$$\omega T = k\lambda$$

$$\Rightarrow \lambda = \frac{2\pi}{k} \cdot \frac{1}{T}$$

$\lambda$  = Distance between a cycle of a wave.

$$\lambda = \frac{2\pi}{k} \quad (\text{m})$$

or since  $k = \omega \sqrt{\mu \epsilon} \Rightarrow \lambda = \frac{2\pi}{\omega \sqrt{\mu \epsilon}} = \frac{2\pi}{2\pi f \sqrt{\mu \epsilon}} = \frac{1}{f \sqrt{\mu \epsilon}} = \frac{v_p}{f}$

$$\Rightarrow \lambda = \frac{v_p}{f}$$

Ex: Find the wavelength of a wave at 2.4 GHz (Wi-Fi)

in air? Ans  $\lambda = \frac{3 \times 10^8 \text{ m/s}}{2.4 \times 10^9 \frac{1}{s}} = \frac{3}{2.4} \times 10^{-1} = 0.125 \text{ m} \Rightarrow \lambda = 125 \text{ mm}$ .

- General plane wave solution has two terms:

$$\vec{E}(z, t) = \underbrace{E_0 \cos(\omega t - kz)}_{\text{Incident wave}} + \underbrace{E_0 \cos(\omega t + kz)}_{\text{Reflected wave}}$$

Wave Solution in Source Free and Lossy Medium:  
 $\vec{J} = \vec{J}_s = 0$   $\sigma \neq 0$  Ex: water, concrete.

The general wave equation is given as

$$\nabla^2 \vec{E} = \frac{1}{\epsilon} (\nabla \cdot \vec{J}) + \mu \sigma \frac{\partial \vec{E}}{\partial t} + \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2}$$

For  $\vec{J} = \vec{J}_s = 0$  (source free) medium, we get

$$\nabla^2 \vec{E} = \mu \sigma \frac{\partial \vec{E}}{\partial t} + \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2}$$

The solution of this equation is: (Assuming a plane wave)

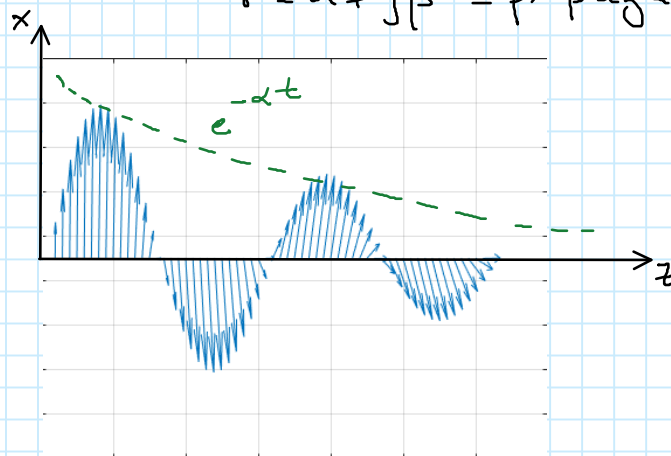
$$\vec{E}(z, t) = E_0 e^{-\alpha z} \cos(\omega t - \beta z)$$

where  $\alpha$  = attenuation constant

$\beta$  = phase constant

and

$\gamma = \alpha + j\beta$  = propagation constant



- For metals,  $\sigma$  is very high, so  $\alpha$  is large. Thus, wave attenuates very quickly. In fact, only surface charge remains.



- The relationship between  $\alpha, \beta$  and  $\sigma$  and other constants are given in the table below ( $\omega = \text{radian frequency} = 2\pi f$ )

E.M. Wave Propagation properties		Exact	Good dielectric $\left(\frac{\sigma}{\omega\epsilon}\right)^2 \ll 1$	Good conductor $\left(\frac{\sigma}{\omega\epsilon}\right)^2 \gg 1$
Attenuation constant $\alpha$	$= \omega\sqrt{\mu\epsilon} \left\{ \frac{1}{2} \left[ \sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2} - 1 \right] \right\}^{1/2}$		$\approx \frac{\sigma}{2} \sqrt{\frac{\mu}{\epsilon}}$	$\approx \sqrt{\frac{\omega\mu\sigma}{2}}$
Phase constant $\beta$	$= \omega\sqrt{\mu\epsilon} \left\{ \frac{1}{2} \left[ \sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2} + 1 \right] \right\}^{1/2}$		$\approx \omega\sqrt{\mu\epsilon}$	$\approx \sqrt{\frac{\omega\mu\sigma}{2}}$
Wave $Z_w$ intrinsic impedances $Z_w = \eta_c$	$= \sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}}$		$= \sqrt{\frac{\mu}{\epsilon}}$	$= \sqrt{\frac{\omega\mu}{2\sigma}} (1 + j)$
Wavelength $\lambda$	$= \frac{2\pi}{\beta}$		$\approx \frac{2\pi}{\omega\sqrt{\mu\epsilon}}$	$\approx 2\pi \sqrt{\frac{2}{\omega\mu\sigma}}$
Velocity $v$	$= \frac{\omega}{\beta}$		$\approx \frac{1}{\sqrt{\mu\epsilon}}$	$\approx \sqrt{\frac{2\omega}{\mu\sigma}}$
Skin depth $\delta$	$= \frac{1}{\alpha}$		$\approx \frac{2}{\sigma} \sqrt{\frac{\epsilon}{\mu}}$	$\approx \sqrt{\frac{2}{\omega\mu\sigma}}$

Ex: X

For a wave at 2.4 GHz (WiFi/WiMax) find the wave velocity, wavelength, attenuation constant and phase constant for a-) in air b-) in sea water c-) in concrete.

Given that:

$$\epsilon_0 = 8.854 \times 10^{-12}, \mu_0 = 4\pi \times 10^{-7}, \epsilon_r |_{\text{sea water}} = 70, \epsilon_r |_{\text{concrete}} = 10$$

and  $\sigma_{\text{air}} = 0, \sigma_{\text{sea water}} = 5 \frac{\text{S}}{\text{m}}, \sigma_{\text{concrete}} = \frac{1}{100} \frac{\text{S}}{\text{m}} = 10^{-2} \frac{\text{S}}{\text{m}}$

Ans

a-) In air:  $\omega = 2\pi f = 2\pi(2.4 \times 10^9) = 1.5 \times 10^{10} = 15 \times 10^9 \text{ rad/s}$

We check the condition for  $\frac{\sigma}{\omega\epsilon} = 0 \Rightarrow \alpha = 0$ .

and  $\beta = \omega\sqrt{\mu\epsilon} = 15 \times 10^9 \sqrt{\mu_0 \epsilon_0} = 15 \times 10^9 \sqrt{(4\pi \times 10^{-7})(8.854 \times 10^{-12})} = 50$

Velocity  $= \frac{\omega}{\beta} = \frac{15 \times 10^9}{50} = 3 \times 10^8 \text{ m/s}$ ,  $\lambda = \frac{2\pi}{\beta} = \frac{2\pi}{50} = \frac{\pi}{25} = 0.125 \text{ m} = 12.5 \text{ cm}$

b-) For water:  $\frac{\sigma}{\omega \epsilon} = \frac{5}{(15 \times 10^9)(70 \times 8.854 \times 10^{-12})} = 0.5378$

$\epsilon_0 \epsilon_r$   $\rightarrow$   $\frac{1}{10}$ th of 1 is considered as " $\ll$ ".

and  $(\frac{\sigma}{\omega \epsilon})^2 = 0.2 \Rightarrow 0.2 \ll 1$ . Thus, we can use good dielectric approximation.

$\Rightarrow \alpha = \frac{\sigma}{2} \sqrt{\frac{\mu}{\epsilon}} = \frac{5}{2} \sqrt{\frac{\mu_0}{\epsilon_0 \epsilon_r}} = \frac{5}{2} \cdot \frac{1}{\sqrt{\epsilon_r}} \sqrt{\frac{\mu_0}{\epsilon_0}} = \frac{5 \cdot 377}{2 \sqrt{70}} = \frac{5 \cdot 377}{2 \cdot 8.3666} = 112.65$

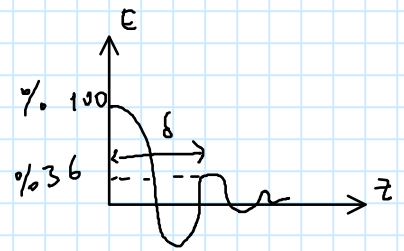
and  $\beta = \omega \sqrt{\mu \epsilon} = \omega \sqrt{\mu_0 \epsilon_0} \cdot \sqrt{\epsilon_r} = 50 \cdot \sqrt{70} = 418$ .

velocity  $v = \frac{1}{\sqrt{\mu \epsilon}} = \frac{1}{\sqrt{\frac{\mu_0 \epsilon_0}{c^2} \epsilon_r}} = \frac{c}{\sqrt{\epsilon_r}} = \frac{3 \times 10^8}{\sqrt{70}} = 3.58 \times 10^7$  m/s.

$\lambda = \frac{2\pi}{\beta} = \frac{2\pi}{418} = 1.5$  cm.

c-)  $(\frac{\sigma}{\omega \epsilon})^2 = \frac{10^{-2}}{(15 \times 10^9)(70 \cdot 8.854 \times 10^{-12})} = 1.15 \times 10^{-6} \ll 1$

HW#4: Complete this example.



### Skin Depth

For lossy mediums, the "skin depth" is the distance for the electromagnetic wave to lose its amplitude by  $\frac{1}{e}$ , where  $e = 2.71828...$

$\Rightarrow$  Define skin depth as:

$\delta = \frac{1}{\alpha}$  (m.)

The proof:

The plane wave expression of an e.m wave in lossy medium is

$\vec{E}(z,t) = \hat{a}_x E_0 e^{-\alpha z} \cos(\omega t - \beta z)$  (Incident wave)  
 $E_0$  (max for when  $z=0$ ).

For  $z = \delta = \frac{1}{\alpha}$

$\vec{E}(z = \delta, t) = \hat{a}_x E_0 e^{-\alpha \frac{1}{\alpha}} \cos(\omega t - \beta z)$   
 $E_0 \cdot \frac{1}{e}$

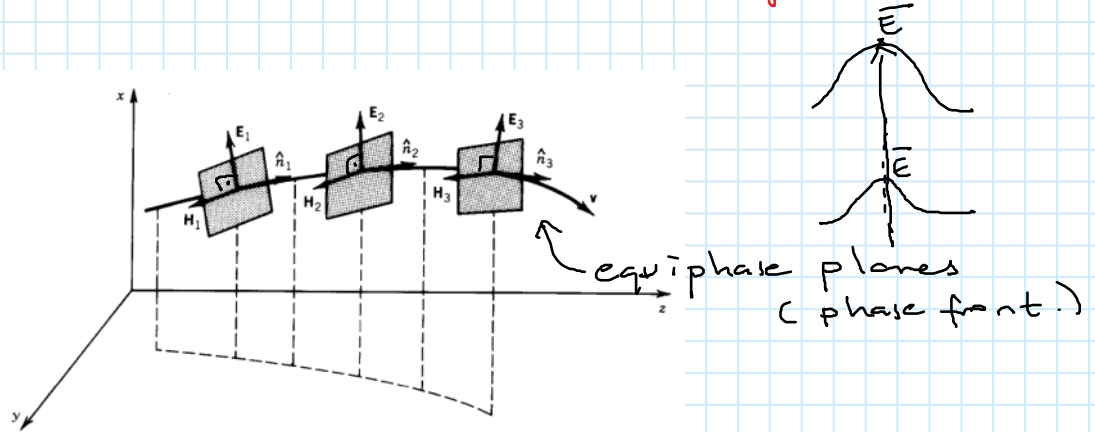
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- Wave Propagation and Plane Waves -

Electromagnetic wave modes are defined as being particular field configurations. They are:

1-) TEM mode = (Transverse Electric and Magnetic)

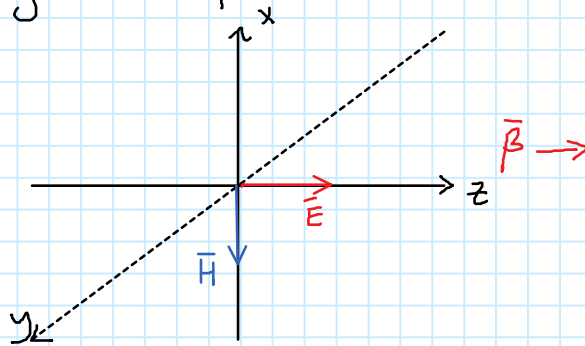


TEM: Transverse Electric and Magnetic. Electric and Magnetic fields are perpendicular to the direction of propagation.

2-) TM Wave - (Transverse Magnetic)

There is no magnetic field in the direction of propagation.

TM<sup>z</sup>: direction of prop.

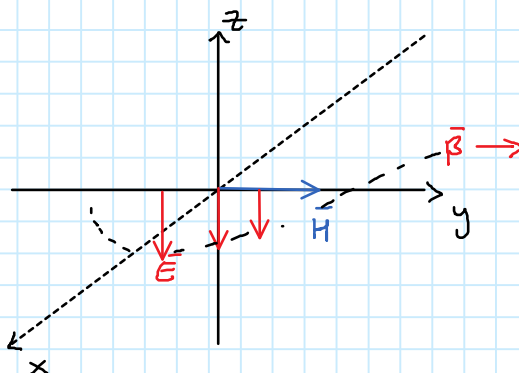


Equiphase plane = xy plane.

3-) TE Wave : (Transverse Electric)

There is no E-field in the direction of propagation.

TE<sup>y</sup>:

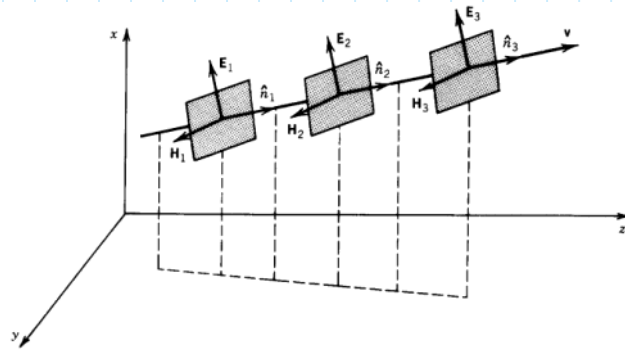


## Plane Wave:

Electric and magnetic fields are contained in a local plane on which waves have equal phase (equiphase plane).

A plane wave

is a TEM wave with planar equiphase surfaces.



Plane Wave

Uniform Plane Wave: Wave amplitudes are uniform over the equiphase plane.

In TEM mode, no  $\vec{E}$  or  $\vec{H}$  are in the direction of propagation.  $\vec{E}$  and  $\vec{H}$  are in the equiphase plane.

- All waves converge to a plane at far away from the source.

## - Plane Wave Equations and Time Harmonic Fields -

$$\vec{E}(z, t) = \hat{a}_x E_0 \cos(\omega t - kz) \quad , \quad k = \text{wave number}$$

- Since Maxwell's equations and the wave equations are linear, and they are in sinusoidal form, we can use "phasors" to simplify our calculations.

$$\Rightarrow \vec{E}(z) = \hat{a}_x E_0 e^{-jkz} \quad (\text{Electric field wave phasor expression.})$$

Similar for magnetic field:

$$\Rightarrow \vec{H}(z) = \hat{a}_y H_0 e^{-jkz} \quad (\text{for plane wave})$$

Time Harmonic

- For plane waves, the general expression in lossless media is:

$$\vec{E}(\vec{R}) = \hat{a}_E E_0 e^{-j\vec{k} \cdot \vec{R}}$$

,  $\hat{a}_E =$  Unit vector in the direction of  $\vec{E}$

where

$\vec{R} =$  Position vector from origin to a point on

equiphase plane  $= \hat{a}_x x + \hat{a}_y y + \hat{a}_z z$

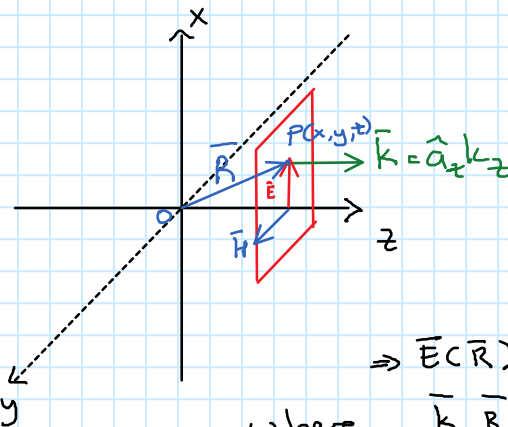
$k =$  Wavenumber vector  $= \hat{a}_x k_x + \hat{a}_y k_y + \hat{a}_z k_z$

Ex:

Use the general expression for a plane wave electric field which is x directed and moving towards z direction

Ans:

$$\vec{k} = \hat{a}_x k_x + \hat{a}_y k_y + \hat{a}_z k_z$$



$$\vec{R} = \hat{a}_x x + \hat{a}_y y + \hat{a}_z z$$

(Wavenumber vector is in the direction of propagation)

$$\Rightarrow \vec{E}(\vec{R}) = \hat{a}_x E_0 e^{-jk_z z} \text{ or } \vec{E}(z) = \hat{a}_x E_0 e^{-jk_z z} \text{ (Phasor)}$$

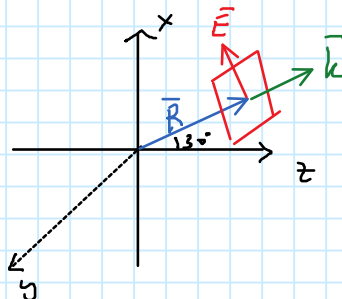
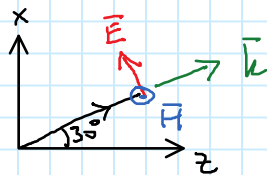
$$\Rightarrow \vec{E}(\vec{R}) = \hat{a}_x E_0 e^{-j\vec{k} \cdot \vec{R}}$$

where  $\vec{k} \cdot \vec{R} = (\hat{a}_z k_z) \cdot (\vec{R}) =$

$$(\hat{a}_z k_z) \cdot (\hat{a}_x x + \hat{a}_y y + \hat{a}_z z) = k_z z$$

Ex. X

Find the electric field expression for a plane wave whose direction of propagation is  $30^\circ$  with the z-axis:

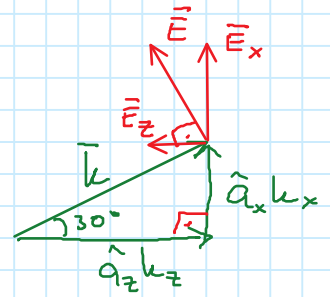


Ans:

Using where

$$\vec{E}(\vec{R}) = \hat{a}_z E_0 e^{-j\vec{k} \cdot \vec{R}}$$

$$\begin{aligned} \vec{k} &= \hat{a}_x k_x + \hat{a}_y k_y + \hat{a}_z k_z = \hat{a}_x k_x + \hat{a}_z k_z \\ &= \hat{a}_x k \sin 30^\circ + \hat{a}_z k \cos 30^\circ \\ &= \hat{a}_x \frac{k}{2} + \hat{a}_z \frac{\sqrt{3}k}{2} \end{aligned}$$

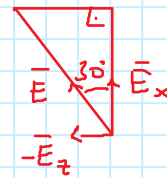


$$\vec{R} = \hat{a}_x x + \hat{a}_y y + \hat{a}_z z$$

$$\Rightarrow \vec{k} \cdot \vec{R} = x \frac{k}{2} + z \frac{k\sqrt{3}}{2}$$

Also,  $\vec{E} = \hat{a}_x E_x - \hat{a}_z E_z$

$E_x = E_0 \sin 30^\circ$   
 $E_z = E_0 \cos 30^\circ$



$$\Rightarrow \vec{E}(\vec{R}) = E_0 \left( \hat{a}_x \frac{\sqrt{3}}{2} - \hat{a}_z \frac{1}{2} \right) e^{-j\vec{k} \cdot \vec{R}} \quad \left( \frac{V}{m} \right) \quad (\text{Phase})$$

- For a plane wave:

$$\vec{H}(\vec{R}) = \frac{1}{\eta} \hat{a}_n \times \vec{E}(\vec{R}) \quad \left( \frac{A}{m} \right)$$

where  $\hat{a}_n$  = Unit vector in the direction of propagation.  
 and  $\eta$  = Point impedance or intrinsic impedance.

and  $\eta = Z_w = \sqrt{\frac{\mu}{\epsilon}}$  (for dielectrics)

For air  $\eta = \sqrt{\frac{\mu_0}{\epsilon_0}} = \sqrt{\frac{4\pi \times 10^{-7}}{8.854 \times 10^{-12}}} = 377 \Omega$ .

For example, in the previous question if we wanted to find  $\vec{H}$ :

$$\hat{a}_n = \frac{\vec{k}}{\|\vec{k}\|} = \frac{\hat{a}_x \frac{k}{2} + \hat{a}_z \frac{\sqrt{3}k}{2}}{\sqrt{\frac{k^2}{4} + \frac{3k^2}{4}}}$$

$$\eta = \omega \sqrt{\mu \epsilon} = \frac{\omega}{c}$$

# P16

Monday, April 5, 2021 4:40 PM

## Wave Power:

Instantaneous wave power density:

$$\vec{P} = \vec{E} \times \vec{H} \quad \left( \frac{W}{m^2} \right)$$

Total wave power,

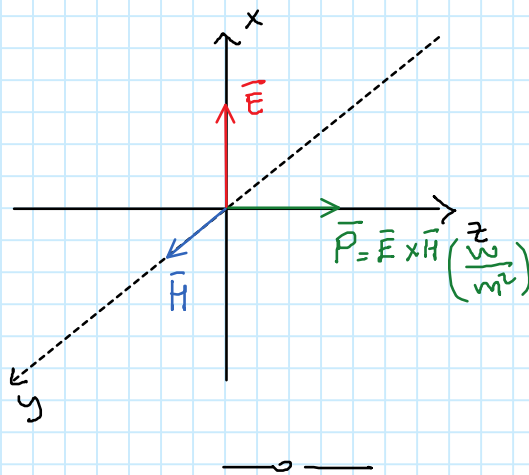
$$P_{total} = \int_{sphere} \vec{P} \cdot d\vec{s} \quad (W)$$

(Poynting vector)

Average Power Density:

$$\vec{P}_{avg} = \frac{1}{2} (\vec{E} \times \vec{H}^*) \quad (W/m^2)$$

$$\vec{P}_{avg} = \vec{E}_{eff} \times \vec{H}_{eff}^* \quad (W/m^2)$$



Ex: X

Find the electric and magnetic field plane waves for  $(\eta = 377 \Omega)$ . Also, find  $\vec{P}$  and  $\vec{P}_{avg}$ .

$$\vec{E} = \hat{a}_x E_0 e^{-jkz} \quad (\text{incident wave}).$$

Ans.

$$\vec{k} = \hat{a}_z k_z \quad (\text{propagation is in the } z\text{-direction}).$$

$$\hat{a}_n = \hat{a}_z$$

⇒

$$\vec{H}(\vec{R}) = \frac{1}{\eta} \hat{a}_n \times \vec{E}(\vec{R})$$

$$= \frac{1}{377} \hat{a}_z \times \hat{a}_x E_0 e^{-jkz}$$

$$= \frac{1}{377} \hat{a}_y E_0 e^{-jkz} = \hat{a}_y \frac{E_0}{377} e^{-jkz}$$

The instantaneous power density vector:



# P17

Monday, April 12, 2021 2:33 PM

$$\bar{P} = \bar{E} \times \bar{H} = \hat{a}_x E_0 e^{-j k z} \times \hat{a}_y \frac{E_0}{\eta} e^{-j k z} = \hat{a}_z \frac{E_0^2}{\eta} e^{-2 j k z} \quad \left( \frac{W}{m^2} \right)$$

Note that

$$\text{Re}[(\bar{E} \times \bar{H}) e^{j \omega t}] \neq \text{Re}[\bar{E} \cdot e^{j \omega t}] \times \text{Re}[\bar{H} \cdot e^{j \omega t}]$$

Because the evaluation of power is non-linear.  
(E is multiplied by H).

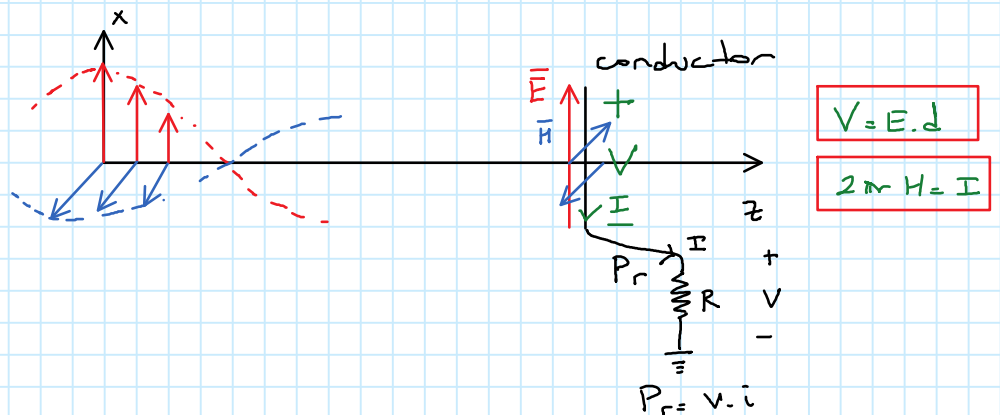
$$\begin{aligned} \Rightarrow P(z, t) &= \text{Re}[\bar{E} \cdot e^{j \omega t}] \times \text{Re}[\bar{H} \cdot e^{j \omega t}] \\ &= \hat{a}_x E_0 \cos(\omega t - k z) \times \hat{a}_y \frac{E_0}{\eta} \cos(\omega t - k z) \\ &= \hat{a}_z \frac{E_0^2}{\eta} \cos^2(\omega t - k z) \\ &= \hat{a}_z \frac{E_0^2}{\eta} \cos(2\omega t - 2kz) \quad \left( \frac{W}{m^2} \right) \quad (\text{Time dependent expression}) \end{aligned}$$

$$P_{avg} = \frac{1}{2} \text{Re}[\bar{E} \times \bar{H}^*] = \frac{E_0^2}{2\eta} \quad \left( \frac{W}{m^2} \right)$$

In case of a lossy media-

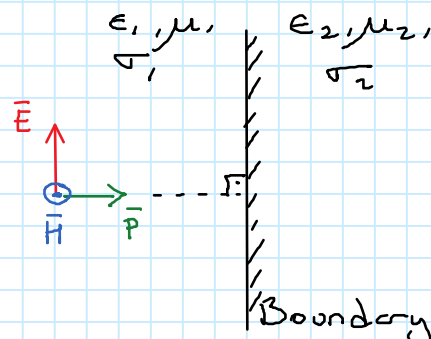
$$P(z, t) = \hat{a}_z \frac{E_0^2}{\eta} e^{-2\alpha z} \cos(2\omega t - 2kz) \quad \left( \frac{W}{m^2} \right)$$

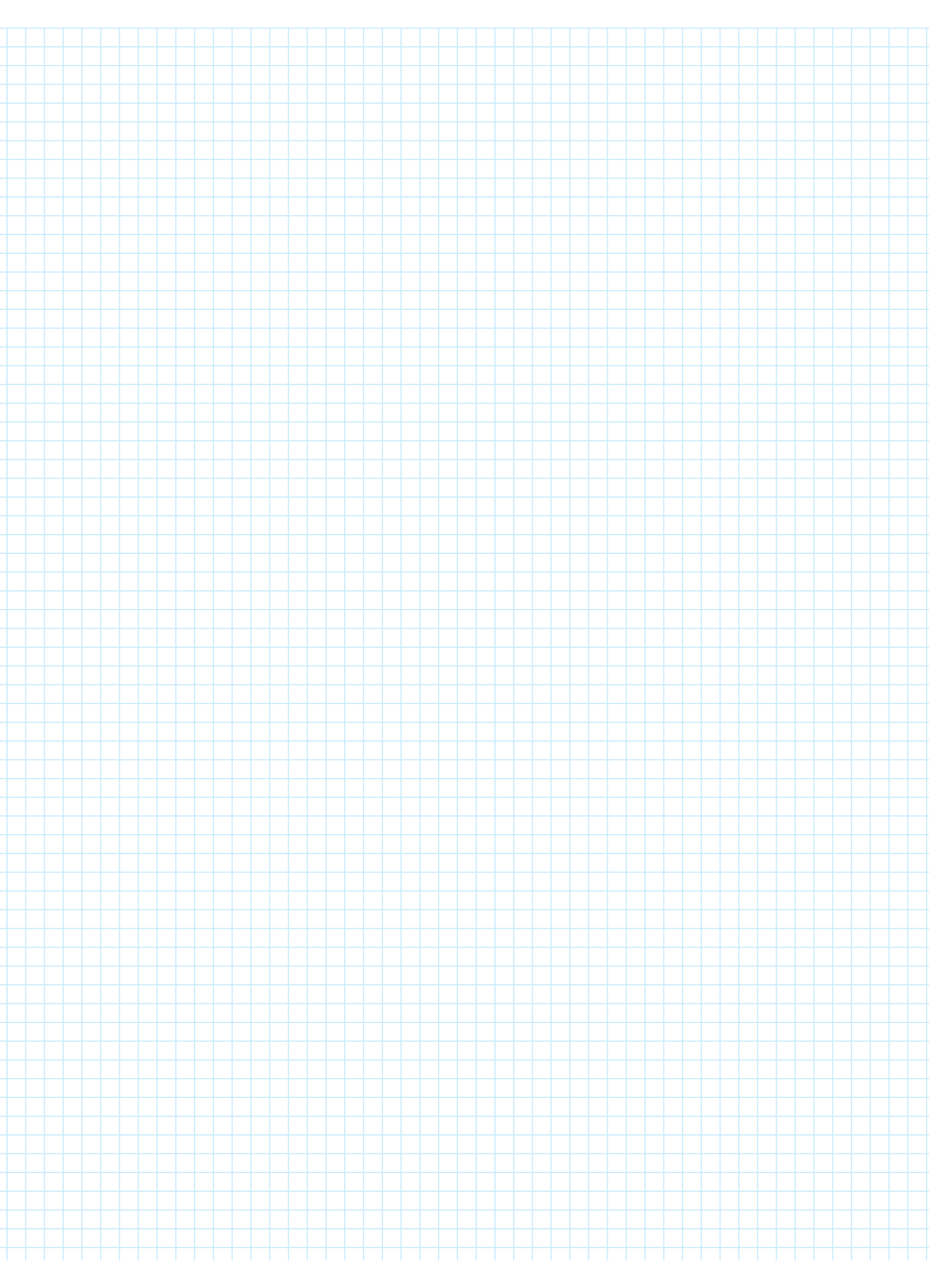
- There is a relation between fields and circuit quantities:



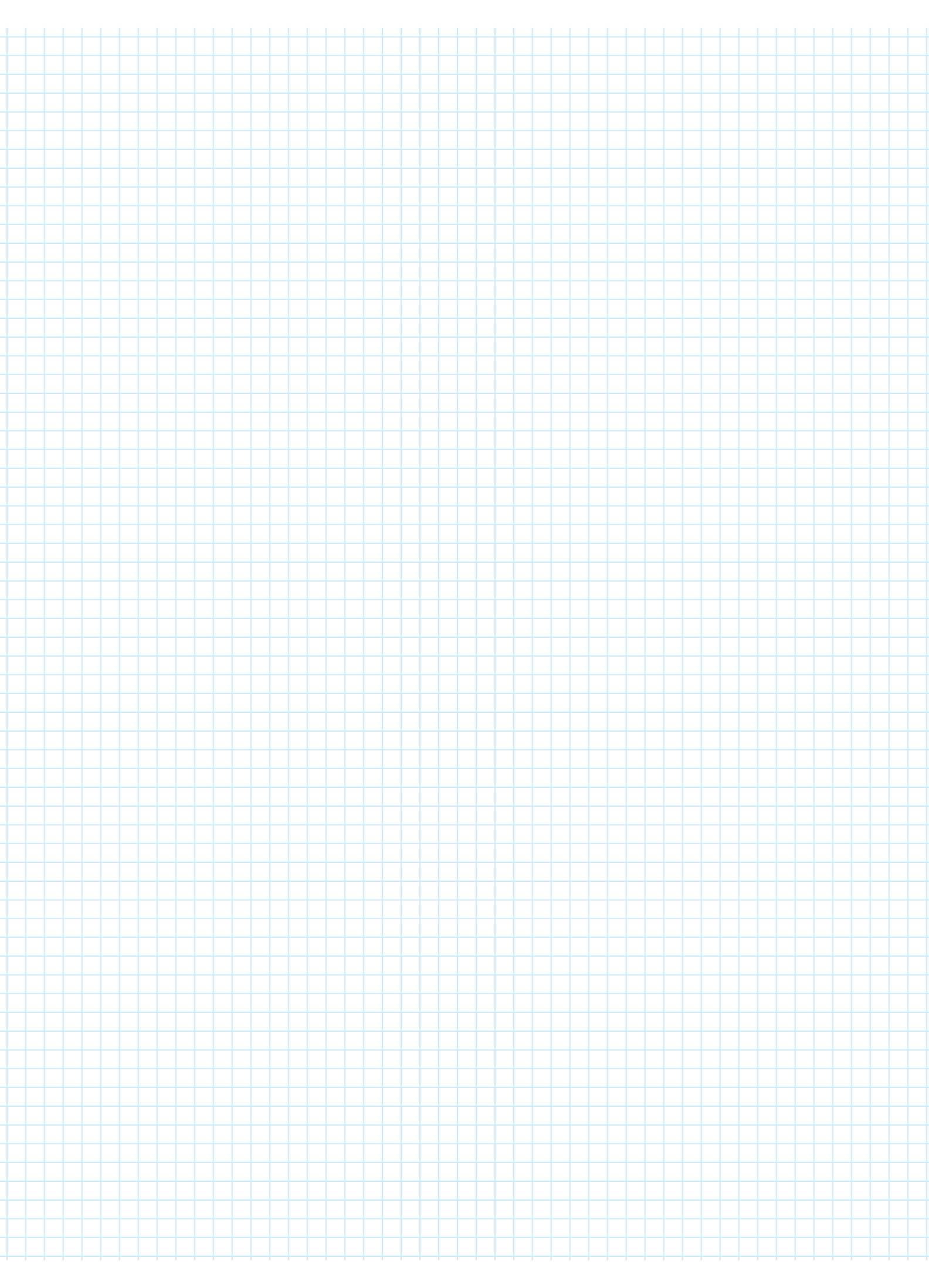
- Reflection and Transmission of Waves -

1-) Normal Interface:  
(Lossless case)



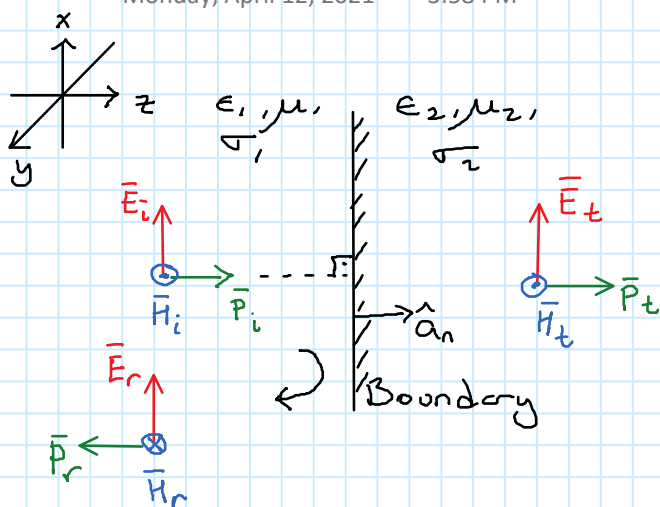


Boundary



# P18

Monday, April 12, 2021 3:58 PM



$$P_r + P_t = P_i \quad (\text{Conservation of power})$$

Analysis:

$$\vec{E}_i = \hat{a}_x E_0 e^{-jk_1 z}, \quad \text{incident wave in lossless medium.}$$

$$\vec{E}_r = \hat{a}_x \Gamma E_0 e^{+jk_1 z}, \quad \text{reflected wave where } k_1 \text{ is the wavenumber of the 1st medium.}$$

where

$$\Gamma = \text{Reflection coefficient} = \frac{E_r}{E_i}$$

$$\text{If } \Gamma = 0 \Rightarrow E_r = 0 \quad (\text{Total transmission})$$

$$\text{If } \Gamma = 1 \Rightarrow E_r = E_i \quad (\text{Total reflection})$$

$$\Rightarrow |\Gamma| = \frac{|\vec{E}_r|}{E_0}, \quad 0 \leq |\Gamma| \leq 1$$

Similarly,

$$\vec{E}_t = \hat{a}_x T E_0 e^{-jk_2 z}, \quad \text{transmitted wave in the 2nd medium.}$$

$$\Rightarrow T = \text{Transmission coefficient} = \frac{E_t}{E_i}, \quad 0 \leq |T| \leq 1$$

Also,

$$\vec{H}_i = \hat{a}_y \frac{E_0}{\eta_1} e^{-jk_1 z}$$

$$\vec{H}_r = -\hat{a}_y \Gamma \frac{E_0}{\eta_1} e^{+jk_1 z}$$

$$\vec{H}_t = \hat{a}_y T \frac{E_0}{\eta_2} e^{-jk_2 z}$$

# P19

Monday, April 12, 2021 4:21 PM

- Imposing the B.C.'s:

$$|E_1^+| = |E_2^+| \Rightarrow |\bar{E}_i| + |\bar{E}_r| = |\bar{E}_t|$$

$$\bar{E}_o + \Gamma \bar{E}_o = T \bar{E}_o$$

$$\boxed{1 + \Gamma = T} \quad (1)$$

- Imposing another B.C.'s:

$$|\bar{H}_1^+| = |\bar{H}_2^+| \Rightarrow \frac{E_o}{\eta_1} - \frac{\Gamma E_o}{\eta_1} = \frac{T E_o}{\eta_2}$$

$$\Rightarrow \boxed{\frac{1}{\eta_1} (1 - \Gamma) = \frac{1}{\eta_2} T} \quad (2)$$

Solving (1) and (2) simultaneously,

$$\Rightarrow \boxed{\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}} \quad \text{and} \quad \boxed{T = \frac{2\eta_2}{\eta_1 + \eta_2}}$$

- Thus, we can obtain  $\Gamma$  and  $T$ , if we know the wave impedances of the mediums

Power Considerations:

$$\bar{P}_{i, \text{avg}} = \frac{1}{2} \text{Re}[\bar{E}_i \times \bar{H}_i^*] = \hat{a}_z \frac{E_o^2}{2\eta_1} \left( \frac{W}{m^2} \right)$$

$$\bar{P}_{r, \text{avg}} = \frac{1}{2} \text{Re}[\bar{E}_r \times \bar{H}_r^*] = -\hat{a}_z |\Gamma|^2 |\bar{P}_{i, \text{avg}}| \left( \frac{W}{m^2} \right)$$

$$\bar{P}_{t, \text{avg}} = \frac{1}{2} \text{Re}[\bar{E}_t \times \bar{H}_t^*] = \hat{a}_z |T|^2 \frac{\eta_1}{\eta_2} \cdot |\bar{P}_{i, \text{avg}}|$$

$$= \boxed{\hat{a}_z [1 - |\Gamma|^2] |\bar{P}_{i, \text{avg}}|}$$

Ex:

A uniform plane wave in air is incident normally upon a flat lossless medium with  $\epsilon_r = 2.56$  (polystyrene). Determine the reflection and transmission coefficients and the power densities in each medium. Assume that the amplitude of the incident E-field is  $1 \text{ mV/m}$

Ans:

$$E_0 = |\bar{E}_i| = 1 \frac{\text{mV}}{\text{m}}$$

$$\text{Wave impedances } Z = \sqrt{\frac{\mu}{\epsilon}} = \eta$$

$$\eta_1 = \sqrt{\frac{\mu_1}{\epsilon_1}} = \sqrt{\frac{\mu_0}{\epsilon_0}} \leftarrow 4\pi \times 10^{-7} \right. \\ \left. \epsilon_0 \leftarrow 8.854 \times 10^{-12} \right.$$

and

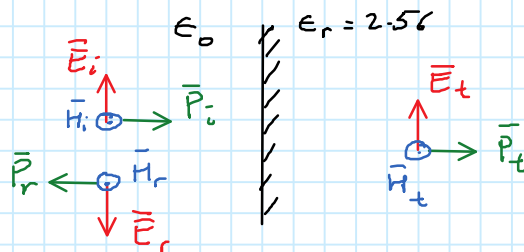
$$\eta_2 = \sqrt{\frac{\mu_2}{\epsilon_2}} = \sqrt{\frac{\mu_0}{2.56\epsilon_0}} = \frac{1}{1.6} \sqrt{\frac{\mu_0}{\epsilon_0}} = \frac{1}{1.6} \eta_1$$

Thus, Reflection &amp; Transmission coefficients are

$$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} = \frac{\frac{1}{1.6} \eta_1 - \eta_1}{\frac{1}{1.6} \eta_1 + \eta_1} = \frac{\frac{1}{1.6} - 1}{\frac{1}{1.6} + 1} = \frac{1 - 1.6}{1 + 1.6} = -0.231$$

$$\Rightarrow T = \frac{2\eta_2}{\eta_1 + \eta_2} = \frac{2 \left( \frac{1}{1.6} \right)}{1 + \frac{1}{1.6}} = \frac{2}{2.6} = 0.769$$

$$\Rightarrow 1 + \Gamma = T \Rightarrow 1 - 0.231 = 0.769 \quad \checkmark \text{ from eqn (1)}$$



Power Calculations.

$$|P_{\text{avg}}^i| = \frac{E_0^2}{2\eta_1} = \frac{(10^{-3})^2}{2(377)} = 1.327 \times 10^{-9} = 1.327 \frac{\text{nW}}{\text{m}^2}$$

$$|P_{\text{avg}}^r| = |\Gamma|^2 |P_{\text{avg}}^i| = (1 - 0.231)^2 (1.327 \times 10^{-9}) = 0.671 \frac{\text{nW}}{\text{m}^2}$$

$$|P_{\text{avg}}^t| = (1 - |\Gamma|^2) |P_{\text{avg}}^i| = |T|^2 \frac{\eta_1}{\eta_2} |P_{\text{avg}}^i| = [1 - (0.231)^2] \cdot (1.327 \times 10^{-9}) \\ \Rightarrow |P_{\text{avg}}^i| = |P_{\text{avg}}^r| + |P_{\text{avg}}^t| = 1.256 \frac{\text{nW}}{\text{m}^2}$$

# P21

Monday, April 19, 2021 2:30 PM

Ex

Repeat the previous example for air to water interface.

$$\epsilon_r |_{\text{water}} = 81, \mu_r |_{\text{water}} = 1 \Rightarrow \mu_{\text{water}} = \mu_0.$$

Ans

$$E_0 = |\bar{E}_i| = 1 \frac{\text{mV}}{\text{m}}.$$

Wave impedances.  $Z = \sqrt{\frac{\mu}{\epsilon}} = \eta.$

$$\eta_1 = \sqrt{\frac{\mu_1}{\epsilon_1}} = \sqrt{\frac{\mu_0}{\epsilon_0}} \leftarrow \frac{4\pi \times 10^{-7}}{8.854 \times 10^{-12}} = 377 \Omega. \quad (\text{impedance of air})$$

and

$$\eta_2 = \sqrt{\frac{\mu_2}{\epsilon_2}} = \sqrt{\frac{\mu_0}{81\epsilon_0}} = \frac{1}{9} \sqrt{\frac{\mu_0}{\epsilon_0}} = \frac{1}{9} \eta_1$$

Thus, Reflection & Transmission coefficients are

$$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} = \frac{\frac{1}{9}\eta_1 - \eta_1}{\frac{1}{9}\eta_1 + \eta_1} = \frac{\frac{1}{9} - 1}{\frac{1}{9} + 1} = \frac{1 - 9}{1 + 9} = -\frac{8}{10} = -0.8$$

$$\Rightarrow T = \frac{2\eta_2}{\eta_1 + \eta_2} = \frac{2(\frac{1}{9})}{1 + \frac{1}{9}} = 0.2$$

Thus,  $|\bar{E}_r| = |\bar{E}_i| |\Gamma| = (1 \text{ mV})(0.8) = 0.8 \text{ mV}$

$|\bar{E}_t| = |\bar{E}_i| |T| = 0.2 \text{ mV}$

$$|P_{\text{avg}}^i| = \frac{E_0^2}{2\eta_1} = \frac{(10^{-3})^2}{2(377)} = 1.327 \times 10^{-9} = 1.327 \frac{\text{nW}}{\text{m}^2}$$

$$|P_{\text{avg}}^r| = |\Gamma|^2 |P_{\text{avg}}^i| = (-0.8)^2 (1.327 \times 10^{-9}) = 8.5 \times 10^{-10} = 0.85 \frac{\text{nW}}{\text{m}^2}$$

$$|P_{\text{avg}}^t| = (1 - |\Gamma|^2) |P_{\text{avg}}^i| = |T|^2 \frac{\eta_1}{\eta_2} |P_{\text{avg}}^i| = [1 - (0.8)^2] \cdot (1.327 \times 10^{-9})$$

$$\Rightarrow |P_{\text{avg}}^t| = |P_{\text{avg}}^r| + |P_{\text{avg}}^t| \quad \checkmark = 0.47 \frac{\text{nW}}{\text{m}^2}$$



Ex:

For the same electric field plane wave with  $E_0 = 1 \frac{mV}{m}$  consider air to aluminum interface. Find  $\Gamma$  and  $T = ?$

For Al  $\rightarrow \sigma = 3.54 \times 10^7 \frac{S}{m}$ ,  $f = 1 \text{ GHz}$  (GSM phone comm.)  
 $\epsilon_r = 10$ .

Ans:

$$\eta_1 = 377 \Omega \text{ (air)}, \eta_2 = ? \Rightarrow \left(\frac{\sigma}{\omega \epsilon}\right)^2 = \left(\frac{3.54 \times 10^7}{2\pi \times 10^9 \times 10 \times 8.854 \times 10^{-12}}\right)^2 \gg 1$$

$$\Rightarrow \eta_2 = \sqrt{\frac{\omega \mu}{2\sigma}} (1+j) = \sqrt{\frac{2\pi \times 10^9 \times 4\pi \times 10^{-7}}{2(3.54 \times 10^7)}} (1+j)$$

$$= 0.015 e^{j0.7854}$$

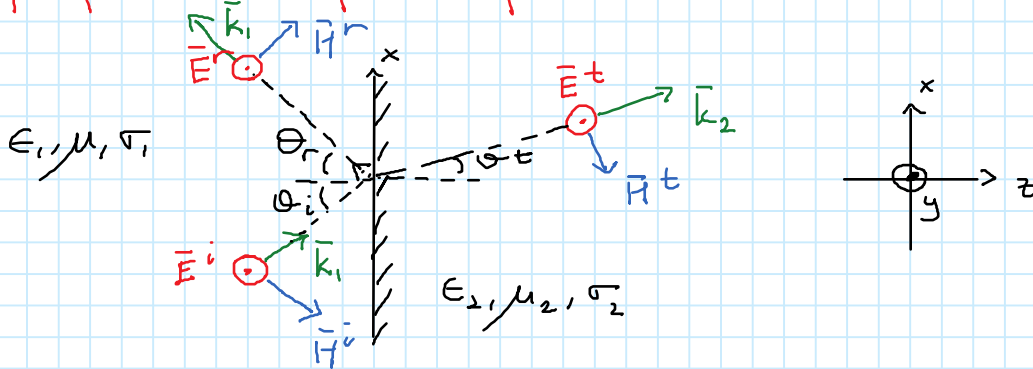
$$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} = \frac{0.015 e^{j0.78} - 377}{0.015 e^{j0.78} + 377} = 0.9999 e^{j3.14 \text{ rad}}$$

$$\begin{aligned} \bar{E}_r &= \bar{E}_i \cdot \Gamma = \hat{a}_x E_0 e^{-jk_z z} \cdot 0.9999 e^{j180^\circ} \\ &= -\hat{a}_x E_0 e^{jk_z z} \end{aligned}$$

2-) Angled Incidence (Oblique Incident) (Lossless Media).

a-) Perpendicular (TE mode) Polarization:  
 shows the directional

properties of the fields.



where  $\theta_i$  = Angle of incidence

$\theta_r$  = Angle of reflection

$\theta_t$  = Angle of transmission

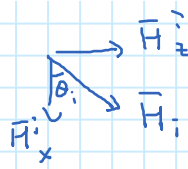
and

$$\bar{E}_i = \hat{a}_y E_0 e^{-j k_1 (x \sin \theta_i + z \cos \theta_i)}$$

$$\begin{aligned} \bar{k}_i &= \hat{a}_x k_x + \hat{a}_z k_z \\ \bar{k}_t &= \hat{a}_x k_x + \hat{a}_y k_y + \hat{a}_z k_z \end{aligned}$$

P23

Monday, April 26, 2021 2:33 PM



$$H_x^i = \hat{a}_x \frac{E_0}{\eta_1} \cos \theta_i$$

$$H_z^i = \hat{a}_z \frac{E_0}{\eta_1} \sin \theta_i$$

$$\bar{H}^i = (-\hat{a}_x \cos \theta_i + \hat{a}_z \sin \theta_i) \frac{E_0}{\eta_1} e^{-j k_1 (x \sin \theta_i + z \cos \theta_i)}$$

where  $\bar{k}_x = \hat{a}_x k_1 \sin \theta_i$ ,  $\bar{k}_z = \hat{a}_z k_1 \cos \theta_i$

$$\bar{E}^r = \hat{a}_y \Gamma_{TE} E_0 e^{-j k_1 (x \sin \theta_i - z \cos \theta_i)}$$

$$\bar{H}^r = (\hat{a}_x \cos \theta_r + \hat{a}_z \sin \theta_r) \Gamma_{TE} \frac{E_0}{\eta_1} e^{-j k_1 (x \sin \theta_i - z \cos \theta_i)}$$

Similarly,

$$\bar{E}^t = \hat{a}_y T_{TE} E_0 e^{-j k_2 (x \sin \theta_t + z \cos \theta_t)}$$

$$\bar{H}^t = (-\hat{a}_x \cos \theta_t + \hat{a}_z \sin \theta_t) \cdot T_{TE} \cdot \frac{E_0}{\eta_2} e^{-j k_2 (x \sin \theta_t + z \cos \theta_t)}$$

Boundary conditions:

$$1-) \bar{E}^i + \bar{E}^r \Big|_{z=0}^{\tan} = \bar{E}^t \Big|_{z=0}^{\tan}$$

$$2-) \bar{H}^i + \bar{H}^r \Big|_{z=0}^{\tan} = \bar{H}^t \Big|_{z=0}^{\tan}$$

There are 2 B.C.'s that give us 4 equations when we equate the real and imaginary parts among themselves. These 4 equations give us the relation among  $\theta_r, \theta_t, \Gamma_{TE}$  and  $T_{TE}$ .

The following relations are obtained:

1-)  $\theta_r = \theta_i$  (Snell's law of reflection)

2-)  $k_1 \sin \theta_i = k_2 \sin \theta_t$  (Snell's law of refraction or transmission)

$k_1$  and  $k_2$  can be obtained from the Table in pg. 9

For lossless dielectrics,  $k_1 = \omega \sqrt{\mu_0 \epsilon_1}$ ,  $k_2 = \omega \sqrt{\mu_0 \epsilon_2}$  ( $\bar{k}$  = wave number)

Also,

$$\Gamma_{TE} = \frac{\eta_2 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$$

$$T_{TE} = \frac{2 \eta_2 \cos \theta_i}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$$

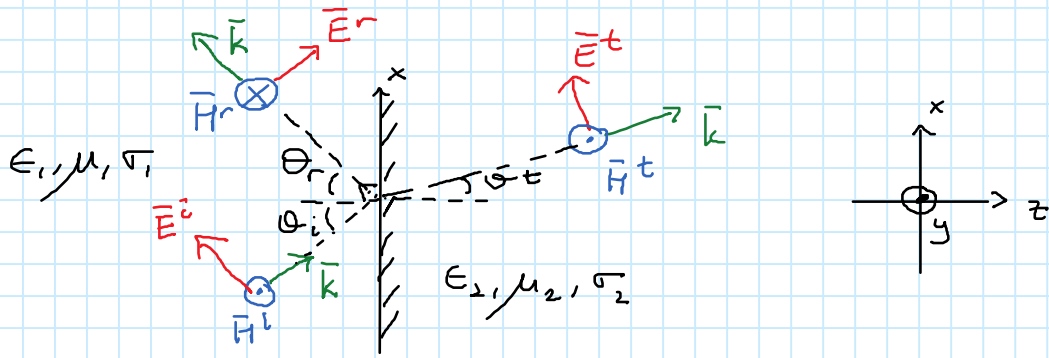
(Fresnel's Transmission Coefficient)

$$\eta_2 \cos \theta_i + \eta_1 \cos \theta_t$$

$$T_{TE} = \frac{2 \eta_2 \cos \theta_i}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$$

} (Fresnel's Transmission Coefficients.)

b-) Parallel (TM) Polarization



where

$$\begin{aligned} \vec{E}^i &= (\hat{a}_x \cos \theta_i - \hat{a}_z \sin \theta_i) E_0 e^{-jk_1(x \sin \theta_i + z \cos \theta_i)} \\ \vec{H}^i &= \hat{a}_y \frac{E_0}{\eta_1} e^{-jk_1(x \sin \theta_i + z \cos \theta_i)} \end{aligned}$$

and

$$\begin{aligned} \vec{E}^r &= (\hat{a}_x \cos \theta_r + \hat{a}_z \sin \theta_r) \Gamma_{TM} E_0 e^{-jk_1(x \sin \theta_r - z \cos \theta_r)} \\ \vec{H}^r &= -\hat{a}_y \Gamma_{TM} \frac{E_0}{\eta_1} e^{-jk_1(x \sin \theta_r - z \cos \theta_r)} \end{aligned}$$

and

$$\begin{aligned} \vec{E}^t &= (\hat{a}_x \cos \theta_t - \hat{a}_z \sin \theta_t) T_{TM} E_0 e^{-jk_2(x \sin \theta_t + z \cos \theta_t)} \\ \vec{H}^t &= \hat{a}_y T_{TM} \frac{E_0}{\eta_2} e^{-jk_2(x \sin \theta_t + z \cos \theta_t)} \end{aligned}$$

Also, after imposing the B.C.'s:

- 1-)  $\theta_r = \theta_i$  (Snell's law of reflection)
- 2-)  $k_1 \sin \theta_i = k_2 \sin \theta_t$  (Snell's law of refraction)

and

$$\Gamma_{TM} = \frac{-\eta_1 \cos \theta_i + \eta_2 \cos \theta_t}{\eta_1 \cos \theta_i + \eta_2 \cos \theta_t}$$

$$T_{TM} = \frac{2\eta_2 \cos \theta_i}{\eta_1 \cos \theta_i + \eta_2 \cos \theta_t}$$

Ex:

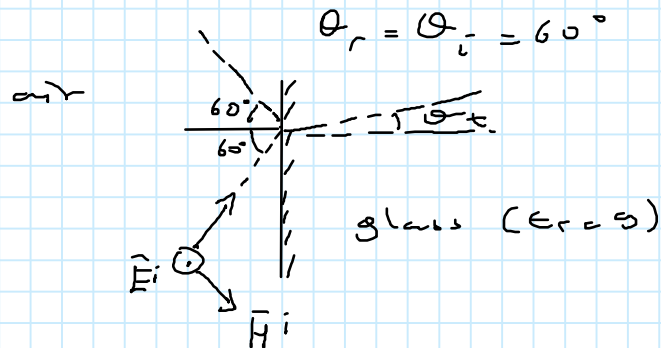
A TE polarized plane wave is incident from air to glass interface ( $\epsilon_r = 9$ ) with an angle of incidence  $60^\circ$

Find the reflection and transmission coefficients

Find the amount of power transferred from medium 1 to medium 2. Given  $E_0 = 1 \frac{\text{mV}}{\text{m}}$ .

Ans:

From the Snell's law of reflection:



From the Snell's law of refraction.

$$k_1 \sin \theta_i = k_2 \sin \theta_t$$

where  $k_1 = \omega \sqrt{\mu_1 \epsilon_1} = \omega \sqrt{\mu_0 \epsilon_0}$

and  $k_2 = \omega \sqrt{\mu_2 \epsilon_2} = \omega \sqrt{\mu_0 \epsilon_{r2} \cdot \epsilon_0} = 3 \omega \sqrt{\mu_0 \epsilon_0}$

↓  
9

Substituting  $k_1$  and  $k_2$  into the Snell's law of refraction,

$$\omega \sqrt{\mu_0 \epsilon_0} \sin \theta_i = 3 \omega \sqrt{\mu_0 \epsilon_0} \sin \theta_t$$

$\frac{\sqrt{3}}{2}$

$$\Rightarrow \sin \theta_t = \frac{\sqrt{3}}{6} \Rightarrow \theta_t = \sin^{-1} \left( \frac{\sqrt{3}}{6} \right) = 16.78^\circ \approx 17^\circ$$

Also,

$$\Gamma_{TE} = \frac{\eta_2 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$$

where

$$\eta_1 = \sqrt{\frac{\mu_1}{\epsilon_1}} = \sqrt{\frac{\mu_0}{\epsilon_0}}, \quad \eta_2 = \sqrt{\frac{\mu_2}{\epsilon_2}} = \sqrt{\frac{\mu_0}{\epsilon_{r2} \epsilon_0}} = \frac{1}{3} \eta_1$$

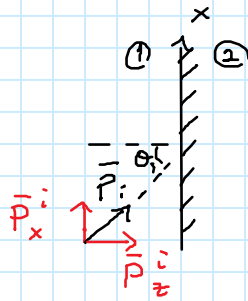
$$\Gamma_{TE} = \frac{\frac{1}{3} \eta_1 \cos 60^\circ - \eta_1 \cos 17^\circ}{\frac{1}{3} \eta_1 \cos 60^\circ + \eta_1 \cos 17^\circ} = \frac{\frac{1}{3} (0.5) - 0.9563}{\frac{1}{3} (0.5) + 0.9563}$$

$$\Rightarrow 1 + \Gamma = T \Rightarrow 1 - 0.7 = T$$

$$\Rightarrow T_{TE} = 0.3$$

$$\Gamma_{TE} = -0.7$$

## Power Analysis.



$$\Gamma_{TE} = -0.7$$

$$T_{TE} = 0.3$$

$$|\bar{P}_{avg}^i| = \frac{1}{2} \operatorname{Re}[\bar{E}^i \times \bar{H}^i]^* = \frac{1}{2} \frac{E_0^2}{\eta_1} \left( \frac{W}{m^2} \right)$$

$$= \frac{1}{2} \frac{(10^{-3})^2}{377} = 1.32 \frac{nW}{m^2}$$

$$|\bar{P}_{z_{avg}}^i| = |\bar{P}_{avg}^i| \cdot \cos \theta_i = (1.32 \frac{nW}{m^2}) \cdot \left( \frac{1}{2} \right) = \boxed{0.66 \frac{nW}{m^2}}$$

$\uparrow$   
 $60^\circ$

$$|\bar{P}_{avg}^r| = \frac{1}{2} \operatorname{Re}[\bar{E}_r \times \bar{H}_r]^* = \frac{1}{2} \frac{E_0^2}{\eta_1} \cdot |\Gamma|^2 = \frac{1}{2} \frac{(10^{-3})^2}{377} (0.7)^2$$

$$= 0.65 nW.$$

$$\Rightarrow |\bar{P}_{z_{avg}}^r| = |\bar{P}_{avg}^r| \cos 60^\circ = (0.65 nW)(0.5) = \boxed{0.325 nW}$$

$$|\bar{P}_{avg}^t| = \frac{1}{2} \frac{E_0^2}{\eta_1} \cdot \frac{\eta_1}{\eta_2} \cdot |T_{TE}|^2 = (1 - |\Gamma|^2) |\bar{P}_{avg}^i| = (1 - 0.49) (1.32 \frac{nW}{m^2})$$

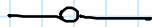
$$= 0.3564 \frac{nW}{m^2}$$

$$\Rightarrow |\bar{P}_{z_{avg}}^t| = (0.3564 \frac{nW}{m^2}) \cdot \cos(\theta_t)$$

$\downarrow$   
 $17^\circ$

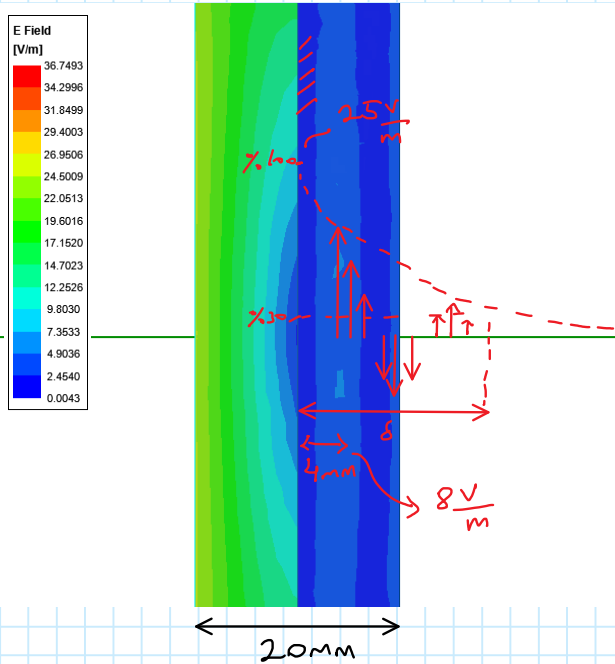
$$= \left( 0.3564 \frac{nW}{m^2} \right) (0.9563) = \boxed{0.3412 \frac{nW}{m^2}}$$

$$0.325 \frac{nW}{m^2} + 0.3412 \frac{nW}{m^2} = 0.66 \frac{nW}{m^2}$$



Simulation of air to water interface (normal incidence at

$$f = 2.46 \text{ GHz}$$



Analysis:

$$\alpha = \sqrt{\frac{\omega \mu_0}{2}}$$

$$= \sqrt{\frac{(2\pi \times 2.4 \times 10^9)(4\pi \times 10^{-7})(5)}{2}}$$

$$= 217.65$$

$$\Rightarrow \delta = \frac{1}{\alpha} = \frac{1}{217.65} = 4.59 \text{ mm}$$

$\Rightarrow$  The simulation

result is in good

agreement with the calculated values.

## 2 Concepts:

1-) Total Transmission:

a-) TE Polarization

$$\Gamma_{TE} = \frac{\eta_2 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t} = 0$$

$$\eta_2 \cos \theta_i - \eta_1 \cos \theta_t = 0$$

or

$$\eta_2 \cos \theta_i = \eta_1 \cos \theta_t$$

or

$$\cos \theta_i = \frac{\eta_1}{\eta_2} \cos \theta_t, \quad \eta_1 = \sqrt{\frac{\mu_1}{\epsilon_1}} \quad \text{and} \quad \eta_2 = \sqrt{\frac{\mu_2}{\epsilon_2}} \quad (\text{drexer})$$

or

$$\cos \theta_i = \sqrt{\frac{\mu_1}{\mu_2} \left( \frac{\epsilon_2}{\epsilon_1} \right)} \cdot \cos \theta_t \quad \text{--- (1)}$$

# P28

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We have also, Snell's law of refraction

$$k_1 \sin \theta_i = k_2 \sin \theta_t$$

or

$$\sin \theta_i = \frac{k_2}{k_1} \sin \theta_t$$

or

$$\sin^2 \theta_i = \left( \frac{k_2}{k_1} \right)^2 \sin^2 \theta_t, \quad k_1 = \omega \sqrt{\mu_1 \epsilon_1}, \quad k_2 = \omega \sqrt{\mu_2 \epsilon_2}$$

or

$$\sin^2 \theta_i = \left( \frac{\mu_2 \sqrt{\mu_2 \epsilon_2}}{\mu_1 \sqrt{\mu_1 \epsilon_1}} \right)^2 \sin^2 \theta_t$$

or

$$\sin^2 \theta_i = \frac{\mu_2 \epsilon_2}{\mu_1 \epsilon_1} \sin^2 \theta_t$$

or

$$\sin^2 \theta_t = \frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2} \sin^2 \theta_i \quad \text{--- (2)}$$

Then, we have

$$\cos \theta_i = \sqrt{\frac{\mu_1}{\mu_2} \left( \frac{\epsilon_2}{\epsilon_1} \right)} \cos \theta_t \quad \text{--- (1)}$$

Take the square of both sides of (1).

$$\cos^2 \theta_i = \frac{\mu_1 \epsilon_2}{\mu_2 \epsilon_1} \cos^2 \theta_t$$

or

$$1 - \sin^2 \theta_i = \frac{\mu_1 \epsilon_2}{\mu_2 \epsilon_1} (1 - \sin^2 \theta_t)$$

Then,

$$1 - \sin^2 \theta_i = \frac{\mu_1 \epsilon_2}{\mu_2 \epsilon_1} \left( 1 - \frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2} \sin^2 \theta_i \right)$$

↳ replace this term by eqn. (2)

Solving for  $\sin \theta_i$  gives

$$\sin \theta_i = \sqrt{\frac{\frac{\epsilon_2}{\epsilon_1} - \frac{\mu_2}{\mu_1}}{\frac{\mu_1}{\mu_2} - \frac{\mu_2}{\mu_1}}}$$

For  $\theta_i$  to exist, the term inside the square root must be less than 1, i.e



$$\frac{\epsilon_2}{\epsilon_1} - \frac{\mu_2}{\mu_1} \leq \frac{\mu_1}{\mu_2} - \frac{\mu_2}{\mu_1}$$

or

$$\boxed{\frac{\epsilon_2}{\epsilon_1} \leq \frac{\mu_1}{\mu_2}} \text{ must hold}$$

If  $\mu_1 = \mu_2 = \mu_0 \Rightarrow$ 

$$\boxed{\epsilon_2 \leq \epsilon_1}$$

However, for  $\mu_1 = \mu_2 = \mu_0$ .

$$\sin \theta_i = \frac{\left| \frac{\epsilon_2 - \mu_2}{\epsilon_1} - \frac{\mu_1}{\mu_2} \right|}{\left| \frac{\mu_1}{\mu_2} - \frac{\mu_2}{\mu_1} \right|} = \infty$$

$\sin \theta_i = \infty$  means that there is no solution  $\Rightarrow$  No such angle exists

b-) TM Pol

$$\Gamma_{TM} = \frac{-\sqrt{\frac{\mu_1}{\epsilon_1}} \cos \theta_i + \sqrt{\frac{\mu_2}{\epsilon_2}} \cos \theta_t}{\sqrt{\frac{\mu_1}{\epsilon_1}} \cos \theta_i + \sqrt{\frac{\mu_2}{\epsilon_2}} \cos \theta_t} = 0$$

If we go through a similar analysis as before

$$\sin \theta_i = \frac{\left| \frac{\epsilon_2 - \mu_2}{\epsilon_1} - \frac{\mu_1}{\mu_2} \right|}{\left| \frac{\epsilon_2}{\epsilon_1} - \frac{\epsilon_1}{\epsilon_2} \right|}$$

$$\Rightarrow \frac{\epsilon_1}{\epsilon_1} - \frac{\mu_2}{\mu_1} \leq \frac{\epsilon_2}{\epsilon_1} - \frac{\epsilon_1}{\epsilon_2} \Rightarrow \boxed{\frac{\mu_2}{\mu_1} \geq \frac{\epsilon_1}{\epsilon_2}} \text{ must hold.}$$

If  $\mu_1 = \mu_2 = \mu_0 \Rightarrow$ 

$$\sin \theta_i = \sqrt{\frac{\frac{\epsilon_2 - 1}{\epsilon_1}}{\frac{\epsilon_2}{\epsilon_1} - \frac{\epsilon_1}{\epsilon_2}}} = \sqrt{\frac{\epsilon_2 - \epsilon_1}{\frac{\epsilon_2^2 - \epsilon_1^2}{\epsilon_1 \epsilon_2}}}$$

$$\text{or } \sin \theta_i = \left[ \frac{\cancel{\epsilon_2} - \cancel{\epsilon_1}}{\cancel{\epsilon_1}} \cdot \frac{\cancel{\epsilon_1} \epsilon_2}{(\epsilon_2 - \epsilon_1)(\epsilon_2 + \epsilon_1)} \right]^{\frac{1}{2}} = \sqrt{\frac{\epsilon_2}{\epsilon_1 + \epsilon_2}}$$

$$\Rightarrow \boxed{\theta_i = \sin^{-1} \left( \sqrt{\frac{\epsilon_2}{\epsilon_1 + \epsilon_2}} \right)}$$

(Angle of total transmission or Brewster angle)

Also it can be written as

$$\theta_i = \tan^{-1} \left( \sqrt{\frac{\epsilon_2}{\epsilon_1}} \right)$$

- Thus, the 2<sup>nd</sup> medium must be denser.

$$1 = \frac{\mu_0}{\mu_0} \geq \frac{\epsilon_1}{\epsilon_2} \quad \rightarrow \text{in terms of polarization}$$

$$\Rightarrow \epsilon_2 \geq \epsilon_1$$

Ex:

A TM pol. plane wave is incident from air to polystyrene ( $\epsilon_r = 2.56$ ) interface with oblique incidence. Find the angle of incidence such that all the wave energy is transmitted.

Ans.

$$\epsilon_1 = \epsilon_0, \quad \epsilon_2 = 2.56 \epsilon_0.$$

$$\Rightarrow \theta_i = \sin^{-1} \left( \sqrt{\frac{2.56 \epsilon_0}{\epsilon_0(1+2.56)}} \right) = \sin^{-1} \left( \sqrt{\frac{2.56}{3.56}} \right) = 58^\circ //$$

Alternatively,

$$\theta_i = \tan^{-1} \left( \sqrt{\frac{\epsilon_2}{\epsilon_1}} \right) = \tan^{-1} \left( \sqrt{\frac{2.56 \epsilon_0}{\epsilon_0}} \right) = 58^\circ //$$

## 2-) Total Reflection

a-) TE Pol.

$$|\Gamma_{TE}| = \left| \frac{\sqrt{\frac{\mu_2}{\epsilon_2}} \cos \theta_i - \sqrt{\frac{\mu_1}{\epsilon_1}} \cos \theta_t}{\sqrt{\frac{\mu_2}{\epsilon_2}} \cos \theta_i + \sqrt{\frac{\mu_1}{\epsilon_1}} \cos \theta_t} \right| = 1 \quad (1)$$

Also,

$$\cos \theta_t = \sqrt{1 - \sin^2 \theta_t} = \sqrt{1 - \frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2} \sin^2 \theta_i}$$

Snell's law of refraction

For  $\theta_t$  to not exist

$$\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2} \sin^2 \theta_i \geq 1$$

This condition makes  $\cos \theta_t$  complex and no solution exists for  $\theta_t$

# P31

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$$\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2} \sin^2 \theta_i \geq 1$$

Solving for  $\theta_i$  gives

$$\theta_i \geq \sin^{-1} \left( \sqrt{\frac{\mu_2 \epsilon_2}{\mu_1 \epsilon_1}} \right) \quad (\text{Condition for all reflection.})$$

for when  $\theta_i = \sin^{-1} \left( \sqrt{\frac{\mu_2 \epsilon_2}{\mu_1 \epsilon_1}} \right)$  is called "critical angle".

The condition

$$\mu_2 \epsilon_2 \leq \mu_1 \epsilon_1 \quad \text{to } \theta_i \text{ to exist}$$

For  $\mu_1 = \mu_2 = \mu_0$

$$\theta_i = \sin^{-1} \left( \sqrt{\frac{\epsilon_2}{\epsilon_1}} \right) \quad \text{critical angle}$$

and the condition becomes

$$\epsilon_2 \leq \epsilon_1$$

- The 1<sup>st</sup> medium must be denser

b-) TM pol.

The critical angle formulations and equations and the conditions are the same as in TE pol.

- Thus, critical angle is polarization independent

Ex1

A TE pol. wave is incident at glass to air interface ( $\epsilon_r = 9$  for glass). Find the angle for all waves to be reflected.

Ans.

$$\epsilon_1 = 9 \epsilon_2, \quad \epsilon_2 = \epsilon_0$$

$$\Rightarrow \theta_i = \theta_c = \sin^{-1} \left( \sqrt{\frac{\epsilon_2}{\epsilon_1}} \right) = \sin^{-1} \left( \sqrt{\frac{1}{9}} \right) = \sin^{-1} \left( \frac{1}{3} \right) \approx 20^\circ$$

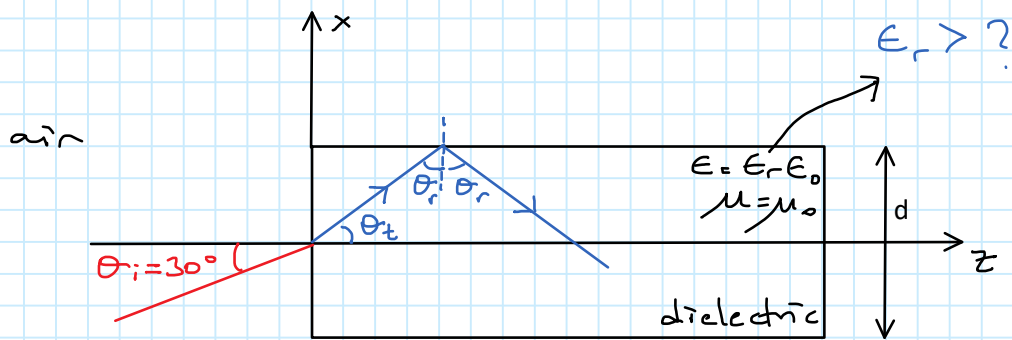
If  $\theta_i \geq \theta_c \Rightarrow$  all energy reflects.

# P32

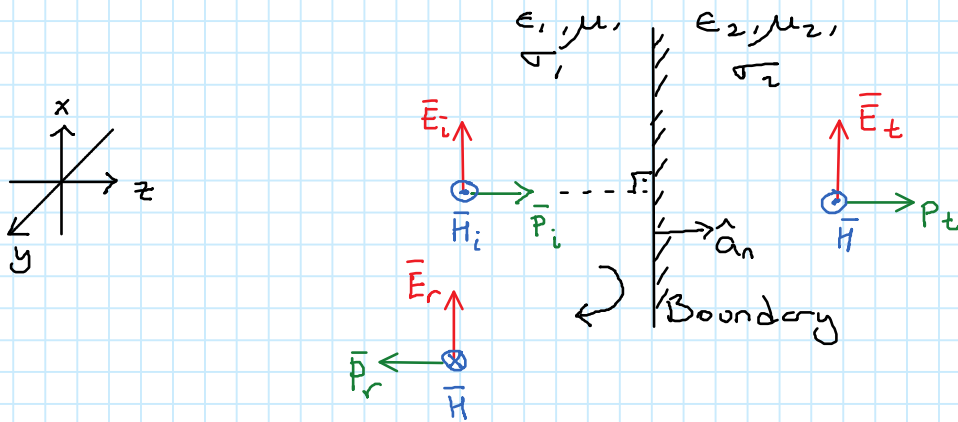
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HW #7:

For a given dielectric cylindrical structure with diameter  $d$ , the plane wave enters the structure from air from its one end. For  $\theta_i = 30^\circ$ , find the required range of dielectr. constant  $\epsilon_r$  for the dielectric material so that the energy is retained inside the structure.



- Normal and Oblique Incidences in Lossy Media -  
 - Normal Incidence:



Writing the expressions for the fields

$$\bar{E}_i = \hat{a}_x E_0 e^{-\alpha_1 z} e^{-j\beta_1 z} \text{ (Phasor)}$$

$$\bar{H}_i = \hat{a}_y \frac{E_0}{\eta_1} e^{-\alpha_1 z} e^{-j\beta_1 z}$$

and 
$$\bar{E}_r = \hat{a}_x \Gamma E_0 e^{+\alpha_1 z} e^{j\beta_1 z}$$

$$\bar{H}_r = -\hat{a}_y \Gamma \frac{E_0}{\eta_1} e^{+\alpha_1 z} e^{j\beta_1 z}$$

Note: For lossy media,

$$\gamma = \alpha + j\beta$$

↑ phase constant

For lossless media,

$$\alpha = 0, \quad k = \text{wavenumber} = \beta$$

# P33

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and 
$$\begin{aligned} \vec{E}_t &= \hat{a}_x T \cdot E_0 e^{-\alpha_2 z} \cdot e^{-j\beta_2 z} \Rightarrow \vec{E}_t(z,t) = \hat{a}_x T E_0 e^{-\alpha_2 z} \cos(\omega t - \beta_2 z) \\ \vec{H}_t &= \hat{a}_y T \frac{E_0}{\eta_2} e^{-\alpha_2 z} \cdot e^{-j\beta_2 z} \end{aligned}$$

and 
$$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}, \text{ where } \eta_1, \eta_2 \text{ are complex from the table in pg. 17.}$$

$$T = \frac{2\eta_2}{\eta_2 + \eta_1}$$

## Power Analysis

$$S_{avg}^i = \hat{a}_z \frac{|E_0|^2}{2} e^{-2\alpha_1 z} \operatorname{Re}\left(\frac{1}{\eta_1^*}\right)$$

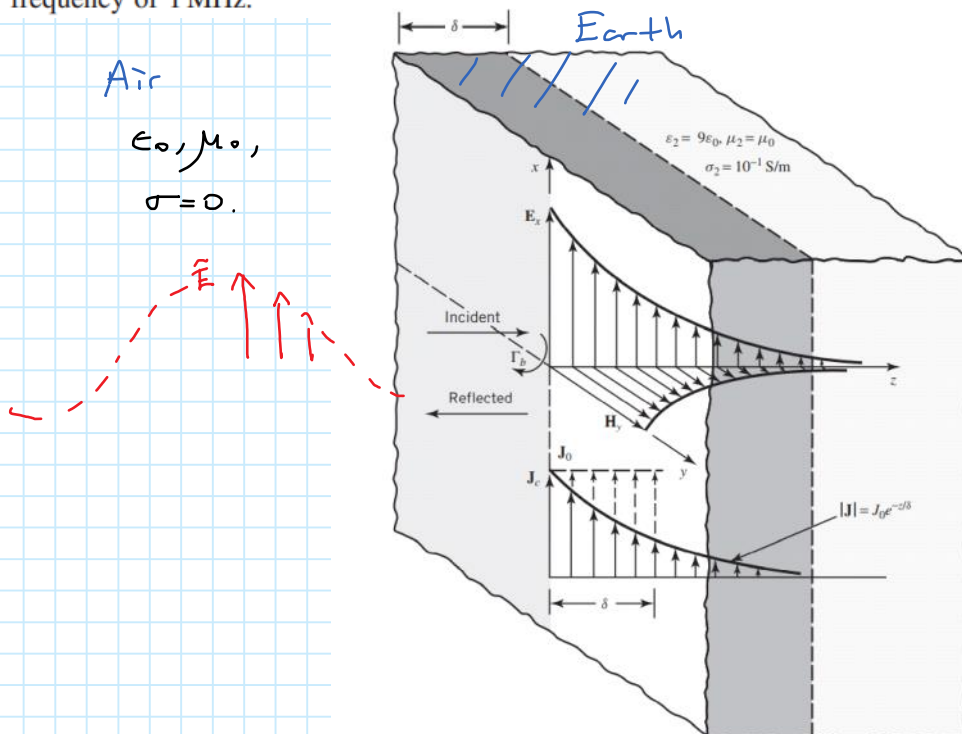
$$S_{avg}^r = -\hat{a}_z |\Gamma|^2 \frac{|E_0|^2}{2} e^{+2\alpha_1 z} \operatorname{Re}\left(\frac{1}{\eta_1^*}\right)$$

$$S_{avg}^t = \hat{a}_z |T|^2 \frac{|E_0|^2}{2} e^{-2\alpha_2 z} \operatorname{Re}\left(\frac{1}{\eta_2^*}\right)$$

where  $\alpha_1, \alpha_2, \beta_1, \beta_2, \eta_1$  and  $\eta_2$  can be computed from the table in pg 17 with constants  $\epsilon_1, \epsilon_2, \mu_1, \mu_2$  and  $\sigma_1$  and  $\sigma_2$  are given.

## Ex

A uniform plane wave, whose incident electric field has an x component with an amplitude at the interface of  $10^{-3}$  V/m, is traveling in a free-space medium and is normally incident upon a lossy flat earth as shown in Figure ~~X~~. Assuming that the constitutive parameters of the earth are  $\epsilon_2 = 9\epsilon_0, \mu_2 = \mu_0, \sigma_2 = 10^{-1}$  S/m, determine the variation of the conduction current density in the earth at a frequency of 1 MHz.



# P34

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Ans

- Find  $\bar{E}_t$

-  $\bar{J}_c = \sigma_2 \cdot \bar{E}_t$  (Ohm's law)

$\Rightarrow$  We need to evaluate  $\Gamma = \frac{2\eta_2}{\eta_2 + \eta_1}$  where  $\eta_1 = 377 \Omega$  and

to find  $\eta_2$ :

We check:  $\left(\frac{\sigma_2}{\omega \epsilon_2}\right)^2 = \left(\frac{10^{-1}}{2\pi(10^6) \cdot (8.854 \times 10^{-12})}\right)^2 = 40000 \gg 1 \Rightarrow$  Good conductor

$$\Rightarrow \eta_2 = \sqrt{\frac{\omega \mu}{2\sigma}} (1+j) = \sqrt{\frac{(2\pi \times 10^6)(4\pi \times 10^{-7})}{2 \times 10^{-1}}} (1+j) = 2\pi (1+j)$$

$$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} = \frac{2\pi(1+j) - 377}{2\pi(1+j) + 377} = 0.567 \angle 178.1^\circ$$

and

$$T = 1 + \Gamma = 1 + 0.567 \angle 178.1^\circ$$

Thus,

$$\begin{aligned} \bar{E}_t &= \hat{a}_x T \cdot E_0 e^{-\alpha_2 z} \cdot e^{-j\beta_2 z} & \text{where } E_0 &= 1 \frac{\text{mV}}{\text{m}} \\ \bar{H}_t &= \hat{a}_y T \frac{E_0}{\eta_2} e^{-\alpha_2 z} \cdot e^{-j\beta_2 z} \end{aligned}$$

$$\Rightarrow |\bar{E}_t| = |T| \cdot |E_0| = 10^{-3} |0.0335 + j0.0321| = 4.64 \times 10^{-5} \frac{\text{V}}{\text{m}}$$

$$\bar{J}_c \Big|_{z=0} = \sigma |\bar{E}_t| = 10^{-1} \left( 4.64 \times 10^{-5} \frac{\text{V}}{\text{m}} \right) = 4.64 \times 10^{-6} \frac{\text{V} \cdot \text{s}}{\text{m}^2}$$

$$\Rightarrow J_0 = 4.64 \mu \frac{\text{A}}{\text{m}^2}$$

$$|\bar{J}_c(z)| = J_0 \cdot e^{-\alpha_2 z} = J_0 \cdot e^{-\frac{z}{\delta}}$$

where

$$\delta = \sqrt{\frac{2}{\omega \mu_2 \sigma_2}} = \sqrt{\frac{2}{2\pi \times 10^6 (4\pi \times 10^{-7}) 10^{-1}}} = 1.59 \text{ m}$$

$$\Rightarrow |\bar{J}_c(z)| \Big|_{z=1.59 \text{ m}} = J_0 \cdot e^{-1} = 0.3679 \cdot J_0 = 0.3679 (4.64 \mu \frac{\text{A}}{\text{m}^2}) = 1.707 \mu \frac{\text{A}}{\text{m}^2}$$

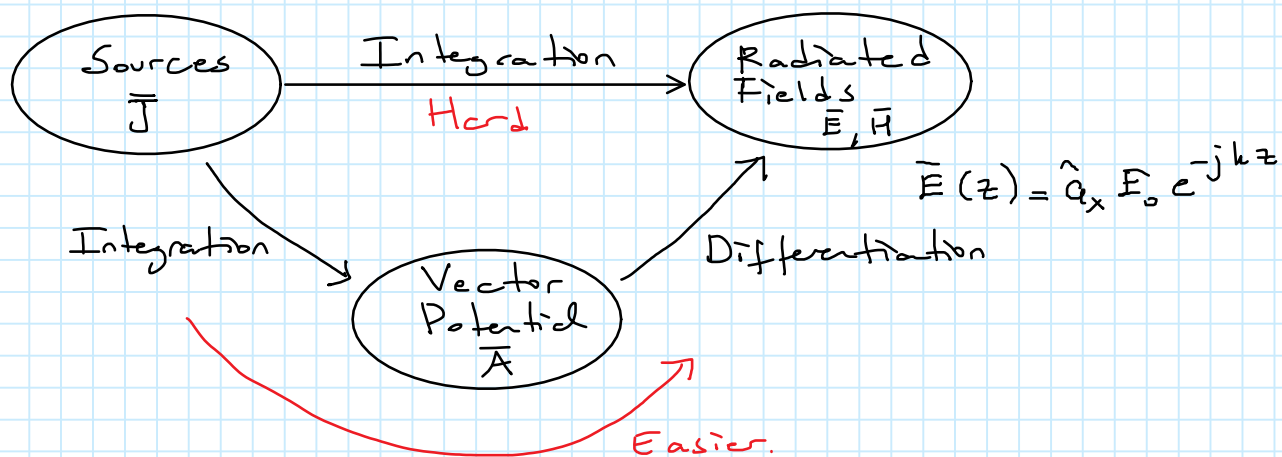
—○—

### - Oblique Incidence:

The formulations of the oblique incidence in lossy media are the same as that of the lossless media with  $\alpha, \beta, \gamma$  and other parameters are functions of  $\sigma$  as in table in ps-9.

### - Radiation -

The problem of radiation can be depicted as in the figure below



Differentiation Path:

$$\vec{E} = -j\omega\vec{A} - j\frac{1}{\omega\epsilon}\nabla(\vec{J}\cdot\vec{A})$$

Integration Path:

$$\vec{A} = \frac{\mu}{4\pi} \int_V \vec{J} \cdot \frac{e^{-jkR}}{R} dv', \quad \vec{J} = \frac{A}{m^2} \quad (\text{volumetric source})$$

or for surface currents (surface source)

$$\vec{A} = \frac{\mu}{4\pi} \int_S \vec{J}_s \cdot \frac{e^{-jkR}}{R} ds', \quad \vec{J}_s = \frac{A}{m} \quad (\text{surface source})$$

or for linear current sources:

$$\vec{A} = \frac{\mu}{4\pi} \int_C \vec{I} \cdot \frac{e^{-jkR}}{R} dl', \quad I = A \quad (\text{current})$$

$$\bar{A} = \frac{\mu}{4\pi} \int_C \bar{I} \cdot \frac{e^{-jkR}}{R} dl', \quad I = A \text{ (current)}$$



Far field approximations ( $R \gg \lambda$ )

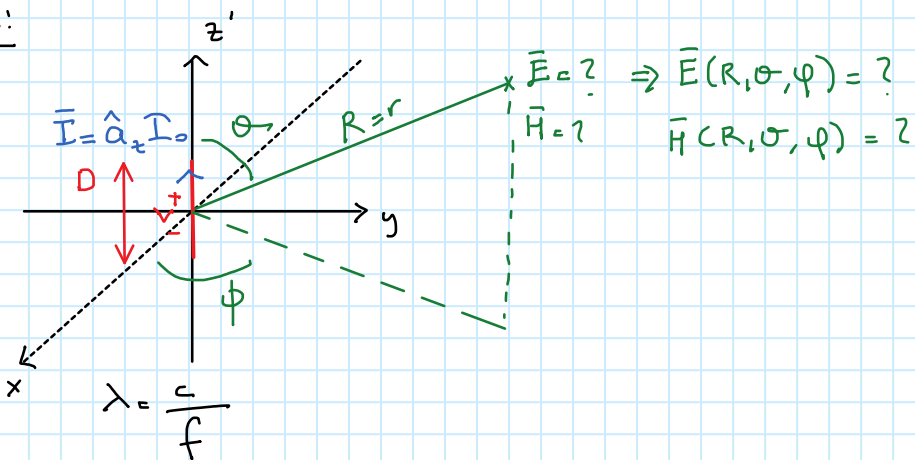
$R=r$  (radial distance from the origin)

$\bar{E} = -j\omega\bar{A}$  for  $E_\theta$  component only  $E_R = 0$

Ex:

Given a very small conductor ( $D \ll \lambda$ ) with a current  $\bar{I} = \hat{a}_z I_0$  (Phasor), find the radiated fields in air?

Ans:



To find A:

$$\bar{A} = \frac{\mu}{4\pi} \int_C \frac{\bar{I} \cdot e^{-jkR}}{R} dl'$$

or

$$\bar{A} = \frac{\mu_0}{4\pi} \int_C (\hat{a}_z I_0) \frac{e^{-jkR}}{r} dz'$$

$$\Rightarrow \bar{A} = \frac{4\pi \times 10^{-7}}{4\pi} \int_{-D/2}^{D/2} \hat{a}_z I_0 \frac{e^{-jkR}}{r} dz'$$

$A_\theta = A_z \sin\theta$

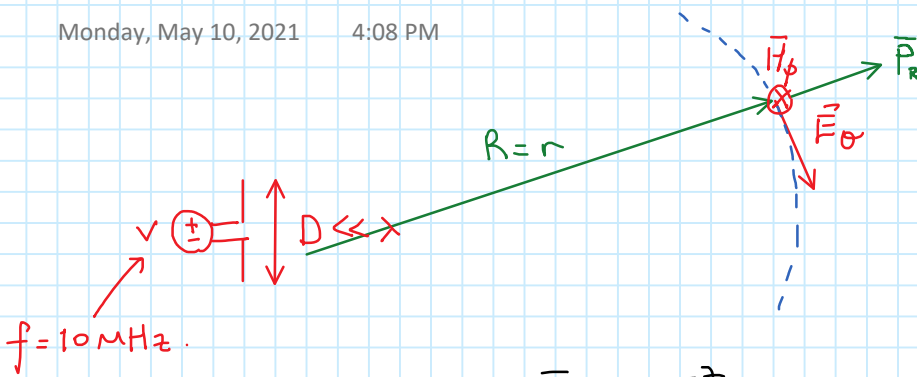
$$\Rightarrow \bar{A} = \hat{a}_z 10^{-7} \cdot I_0 \cdot \frac{e^{-jkR}}{r} \cdot D$$

$$\Rightarrow \bar{E} = -j\omega\bar{A}_\theta \Rightarrow \bar{E}_\theta = -j\omega 10^{-7} \cdot I_0 \frac{e^{-jkR}}{r} \cdot D \cdot \sin\theta \quad \left(\frac{V}{m}\right)$$

$$\text{or } \bar{E}_\theta = 10^{-7} \omega I_0 \cdot D \cdot \sin\theta \frac{e^{-jkR}}{r} e^{-j\frac{\pi}{2}}$$

$$\bar{E}_\theta(r,t) = \text{Re}[\bar{E}_\theta \cdot e^{j\omega t}] = \underbrace{10^{-7} \omega I_0 \cdot D \cdot \frac{1}{r} \sin\theta}_{E_0} \cos\left(\omega t - kr - \frac{\pi}{2}\right)$$

Phase factor



$f = 10 \text{ MHz}$

$$\lambda = \frac{c}{f} = \frac{3 \times 10^8}{10 \times 10^6} = 30 \text{ m}$$

$D \ll 30 \text{ m}$ .  $D = 1 \text{ m}$  ✓

$$\vec{E}_0 = 10^{-7} \omega I_0 \cdot D \cdot \frac{e^{-jkr}}{r} e^{-j\frac{\pi}{2}} \text{ (Phasor)}$$

$$\vec{E}_0 = 10^{-7} \omega I_0 \cdot D \cdot \frac{1}{r} \cos(\omega t - kr - \frac{\pi}{2})$$

phase factor

$$\Rightarrow \vec{H}(r) = \frac{1}{\eta} \hat{a}_n \times \vec{E}(r)$$

$$= \frac{1}{\eta} \cdot \hat{a}_n \times \vec{E}_0$$

$$= \hat{a}_\phi \frac{10^{-7} \omega I_0 D}{\eta} \frac{1}{r} \cos(\omega t - kr - \frac{\pi}{2})$$

$$\vec{P} = \vec{E} \times \vec{H} \text{ (W/m}^2\text{)} \Rightarrow \text{in } \hat{a}_r \text{ direction}$$

Ex:

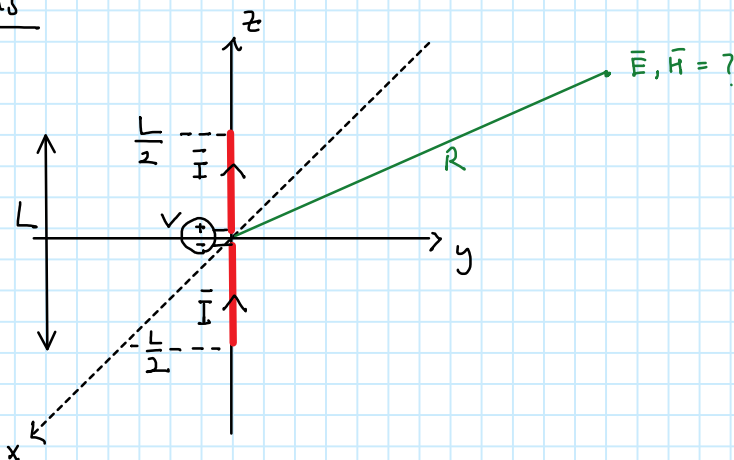
Finite length conductor is used

The current density is given as

$$\vec{I}(z') = \begin{cases} \hat{a}_z I_0 \sin[k(\frac{L}{2} - z')] & , 0 \leq z' \leq L/2 \\ \hat{a}_z I_0 \sin[k(\frac{L}{2} + z')] & , -\frac{L}{2} \leq z' \leq 0 \end{cases}$$

Find the radiated fields at far away from the conductor. frequency = 1 GHz.

Ans



Analysis of  $I(z')$

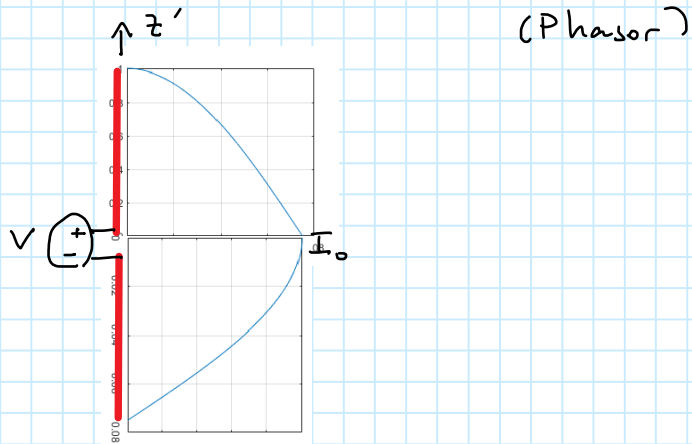
$$\bar{I}(z') = \begin{cases} \hat{a}_z I_0 \sin \left[ k \left( \frac{L}{2} - z' \right) \right], & 0 \leq z' \leq L/2 \\ \hat{a}_z I_0 \sin \left[ k \left( \frac{L}{2} + z' \right) \right], & -\frac{L}{2} \leq z' \leq 0 \end{cases}$$

$$\lambda = \frac{c}{f} = \frac{3 \times 10^8}{1 \times 10^9} = 0.3 = 30 \text{ cm}$$

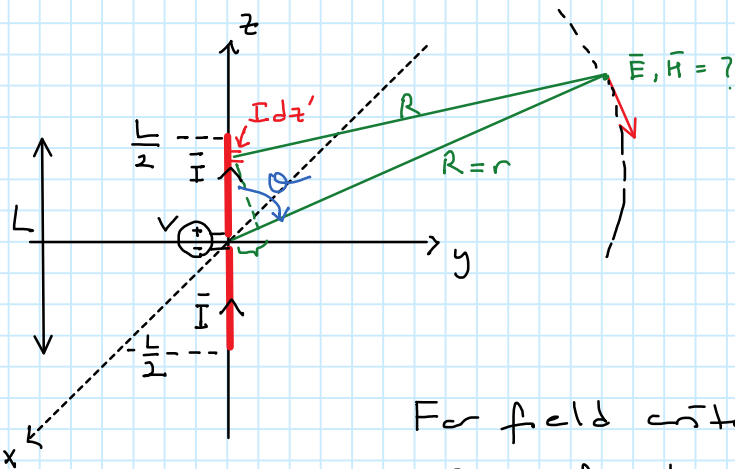
$$k = \text{wave number} = \frac{2\pi}{\lambda} = \frac{2\pi}{0.3} = \frac{2\pi}{\frac{3}{10}} = \frac{20\pi}{3}$$

$L = \text{Conductor length} = \frac{\lambda}{2} = 15 \text{ cm}$  (Half-wave dipole)

$$\Rightarrow \bar{I}(z') = \begin{cases} \hat{a}_z I_0 \sin \left[ \frac{2\pi}{\lambda} \left( \frac{\lambda}{2} - z' \right) \right], & 0 \leq z' \leq L/2 \\ \hat{a}_z I_0 \sin \left[ \frac{2\pi}{\lambda} \left( \frac{\lambda}{2} + z' \right) \right], & -\frac{L}{2} \leq z' \leq 0 \end{cases}$$



Finding  $\bar{A}$  from  $\bar{I}(z')$



$$\bar{A} = \frac{\mu}{4\pi} \int_C \frac{\bar{I} \cdot e^{-jkR}}{R} dl'$$

$$\Rightarrow \bar{A} = \frac{\mu}{4\pi} \int_0^{L/2} \bar{I}(z') \frac{e^{-jkR}}{R} dz' + \frac{\mu}{4\pi} \int_{-L/2}^0 \bar{I}(z') \frac{e^{-jkR}}{R} dz'$$

For field criteria,  $R \gg L$ .

$R = r$  for denominator term

$R = r - z' \cos \theta$  for the phase term

The integral gives  $\bar{A} = \hat{a}_z \eta \frac{I_0 e^{-jkr}}{\omega 2\pi r} \left[ \frac{\cos(\frac{kL}{2} \cos \theta) - \cos(\frac{kL}{2})}{\sin \theta} \right]$

# P39

Monday, May 17, 2021 3:23 PM

and  $\vec{E} = -j\omega A$

$$\Rightarrow \vec{E}_\theta = j\eta \frac{I_0 e^{-jkr}}{2\pi r} \left[ \frac{\cos(\frac{kl}{2} \cos\theta) - \cos \frac{kl}{2}}{\sin\theta} \right] \left( \frac{V}{m} \right)$$

$$H_\phi = j \frac{I_0 e^{-jkr}}{2\pi r} \left[ \frac{\cos(\frac{kl}{2} \cos\theta) - \cos \frac{kl}{2}}{\sin\theta} \right] \left( \frac{A}{m} \right)$$

$$\vec{P}_{avg} = \hat{a}_R \left( \eta \frac{I_0}{2\pi r} \right)^2 / 2\eta \left( \frac{W}{m^2} \right) \quad \vec{P}_{avg} = \frac{|E_\theta|^2}{2\eta}$$

↳ This is the average power

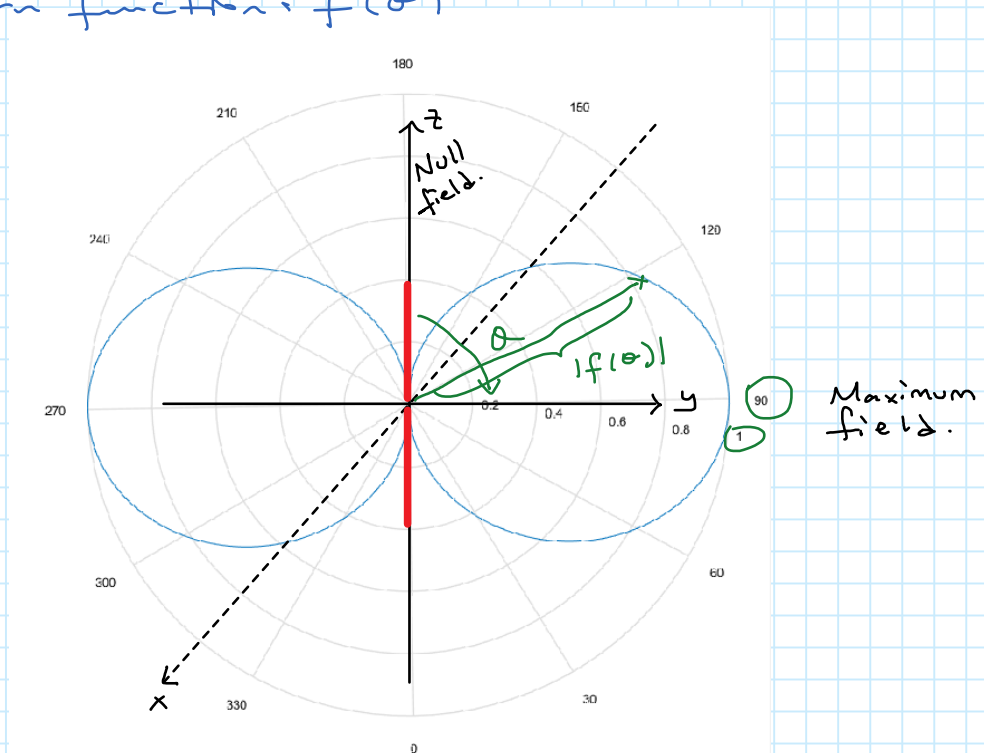
assuming that

$$f(\theta) = \left[ \frac{\cos(\frac{kl}{2} \cos\theta) - \cos \frac{kl}{2}}{\sin\theta} \right] = 1 \text{ (maximum)}$$

where  $f(\theta)$  is the part of the field containing angular dependence.

⇒  $f(\theta) =$  Pattern function (Radiation pattern function)

Pattern function:  $f(\theta)$

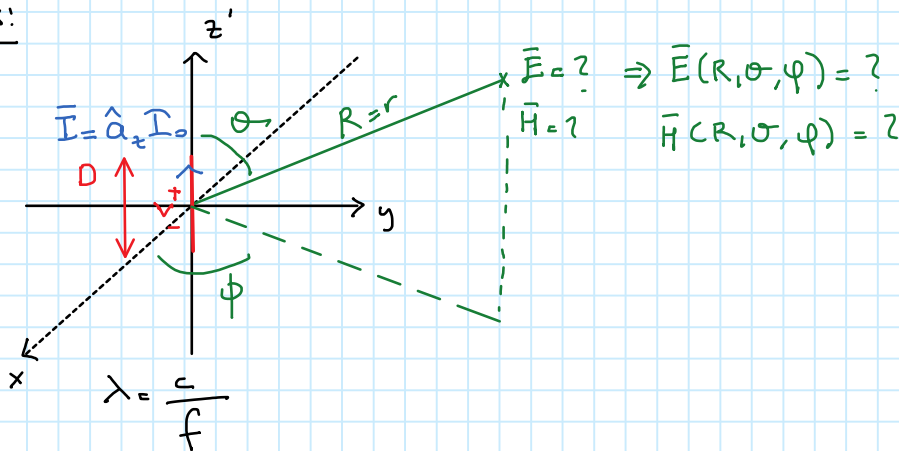


$f(\theta)$  for  $L = \frac{\lambda}{2}$  (Half-wave dipole)

X Ex:

Given a very small conductor ( $D \ll \lambda$ ) with a current  $\bar{I} = \hat{a}_z I_0 z^2$  (Phasor), find the radiated fields in air?

Ans:



To find A:

$$\bar{A} = \frac{\mu}{4\pi} \int_C \frac{\bar{I} \cdot e^{-jkR}}{R} dl'$$

or

$$\bar{A} = \frac{\mu_0}{4\pi} \int_C (\hat{a}_z I_0) \frac{e^{-jkR}}{r} dz'$$

$$\Rightarrow \bar{A} = \frac{4\pi \times 10^{-7}}{4\pi} \int_{-D/2}^{D/2} \hat{a}_z I_0 z^2 \frac{e^{-jkR}}{r} dz'$$

$$\int_{-\frac{D}{2}}^{\frac{D}{2}} z^2 dz = \left. \frac{1}{3} z^3 \right|_{-\frac{D}{2}}^{\frac{D}{2}} = \frac{1}{12} D^3$$

$$\Rightarrow \bar{A} = \hat{a}_z 10^{-7} \cdot I_0 \cdot \frac{e^{-jkR}}{r} \cdot \frac{D^3}{12}$$

$$\Rightarrow \bar{E} = -j\omega \bar{A}_\theta \Rightarrow \bar{E}_\theta = -j\omega 10^{-7} \cdot I_0 \frac{e^{-jkR}}{r} \cdot \frac{D^3}{12} \sin\theta \left(\frac{V}{m}\right)$$

or

$$\bar{E}_\theta = 10^{-7} \omega I_0 \cdot D \cdot \sin\theta \frac{e^{-jkR}}{r} e^{-j\frac{\pi}{2}}$$

$f(\theta) =$  Pattern function.

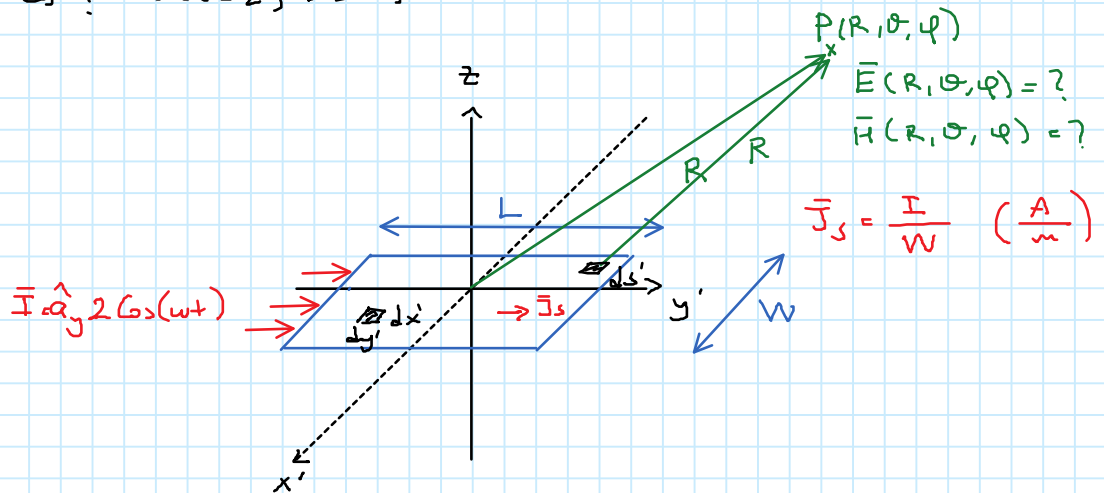
$$\bar{E}_\theta(r, t) = \text{Re}[\bar{E}_\theta \cdot e^{j\omega t}] = \underbrace{10^{-7} \omega I_0 \cdot \frac{D^3}{12} \cdot \frac{1}{r} \cdot \sin\theta}_{E_0} \cdot \underbrace{\cos(\omega t - kr - \frac{\pi}{2})}_{\text{phase factor}}$$

## Midterm Exam Information:

- Midterm exam will be held on 06/08/2021 Friday at 13:30 usual lecture time.
- The exam will be open notes.
- Mobile phones and computers are not allowed to be used during the exam. However, you may use a standard calculator.
- The exam will be online with open-camera.
- During the exam, your hands and paper must be visible on the screen.

Ex:

Given a rectangular sheet with dimensions  $W$  and  $L$ , a current of  $2A$  at  $f=16\text{Hz}$  is fed from its one end. Find the radiated  $\vec{E}$  and  $\vec{H}$  fields? ( $W=2, L=2$ )

Ans:

$$\Rightarrow \vec{J}_s = \hat{a}_y \frac{I}{W} = \hat{a}_y 1 \left( \frac{A}{m} \right)$$

First, find  $\vec{A}$  from  $\vec{J}_s$ :

$$\vec{A} = \frac{\mu_0}{4\pi} \int_S \vec{J}_s \cdot \frac{e^{-jkr}}{R} ds' \quad \hookrightarrow dx' dy'$$

If  $R \gg D = WL$

$\Rightarrow R = r$  (constant)

$$\Rightarrow \vec{A} = \frac{\mu_0}{4\pi} \int_{-\frac{L}{2}}^{\frac{L}{2}} \int_{-\frac{W}{2}}^{\frac{W}{2}} \hat{a}_y \cdot 1 \cdot \frac{e^{-jkr}}{r} dx' dy'$$

$$\bar{A} = \frac{\mu_0}{4\pi} \int_{-\frac{L}{2}}^{\frac{L}{2}} \int_{-\frac{w}{2}}^{\frac{w}{2}} \hat{a}_y \cdot \frac{e^{-jk_r}}{r} dx' dy'$$

$$\Rightarrow \bar{A} = \hat{a}_y \frac{\mu_0}{4\pi} \frac{e^{-jk_r}}{r} \underbrace{\int_{-\frac{L}{2}}^{\frac{L}{2}} \int_{-\frac{w}{2}}^{\frac{w}{2}} dx' dy'}_{w \cdot L = \frac{1}{2} m^2}$$

$$\bar{A} = \hat{a}_y \underbrace{\frac{\mu_0}{4\pi}}_{A_y} \frac{e^{-jk_r}}{r}$$

$$\Rightarrow \bar{E} = -j\omega \bar{A}$$

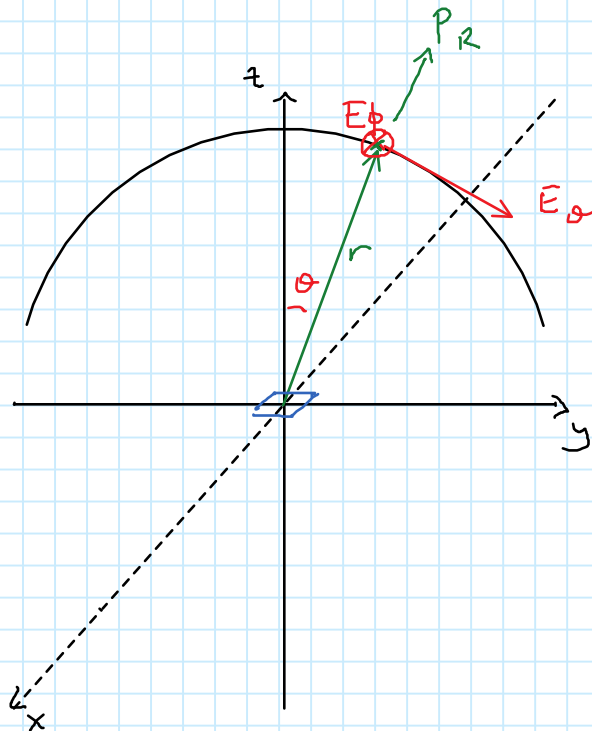
↑  
θ or φ coord.

Thus,  $A_\theta = A_y \cos\theta \sin\phi = \frac{\mu_0}{4\pi} \frac{e^{-jk_r}}{r} \cos\theta \sin\phi$ ,  $A_\phi = A_y \cos\phi = \frac{\mu_0}{4\pi} \frac{e^{-jk_r}}{r} \cos\phi$ .

$$\Rightarrow E_\theta = -j\omega A_\theta, E_\phi = -j\omega A_\phi$$

$$E_\theta = \frac{\mu_0}{4\pi} \underbrace{\cos\theta \sin\phi}_{f(\theta, \phi)} \frac{e^{-jk_r}}{r} \left(\frac{V}{m}\right) \text{ (Phasor)}$$

$$E_\phi = \frac{\mu_0}{4\pi} \underbrace{\cos\phi}_{f(\phi)} \frac{e^{-jk_r}}{r} \left(\frac{V}{m}\right) \text{ (Phasor)}$$

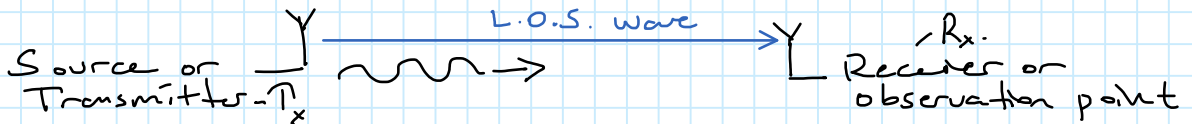


- Electromagnetic Wave Propagation -

In general, there are 3 types of wave propagation -

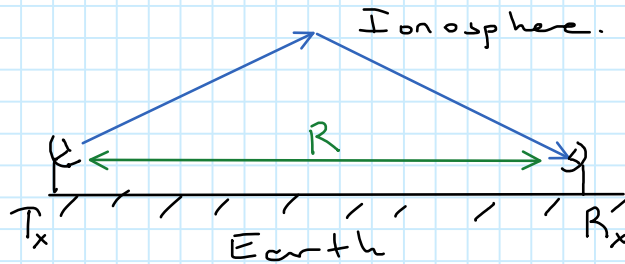
1-) Direct Wave: (Line of Sight Propagation)

- In this propagation, there are no obstacles in between the transmitter and the receiver antennas



2-) Sky Wave (Ionosphere Propagation)

- The source is directed towards the sky, and the waves are reflected from the ionosphere



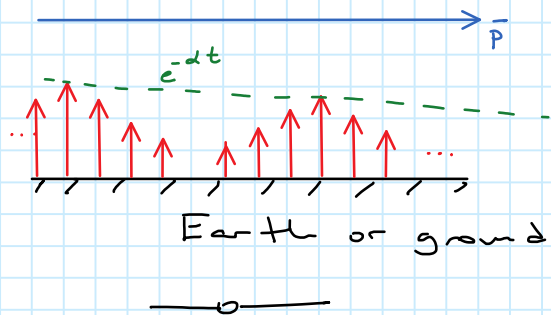
- Long range communication is possible (R is very large)

- Waves are reflected from the ionosphere

3-) Ground Wave (Surface Waves) Propagation.

- These waves can be parallel or perpendicular to ground

- Ground waves move parallel to earth surface with attenuation





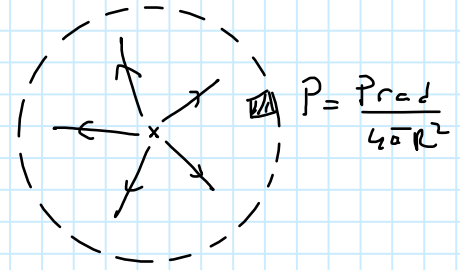
1-) Direct Wave Propagation.

The power density of an isotropic (equally in all directions) source is:

$$P = \frac{P_{rad}}{4\pi R^2} \left( \frac{W}{m^2} \right)$$

Isotropic radiated power density ( $W/m^2$ )

$P_{rad}$  = Total radiated power (W)



In reality the sources (antennas) are not isotropic. They radiate more power in certain directions than the others

Power density of such a source is:

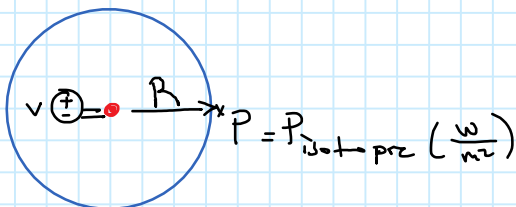
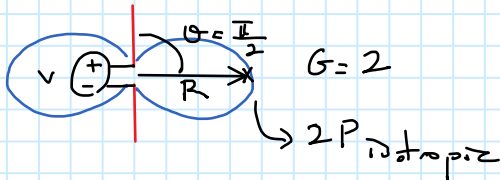
$$P(\theta, \phi) = \frac{P_{rad}}{4\pi R^2} \cdot G(\theta, \phi) \left( \frac{W}{m^2} \right)$$

$P_{iso}$  = Isotropic rad power density direction  
Gain of the source in  $\theta, \phi$  direction

- Unless stated otherwise,  $\theta$  and  $\phi$  are the angles which make  $G(\theta, \phi)$  maximum

$$\text{Antenna Gain} = \frac{P(\theta, \phi)}{P_{isotropic}}$$

Ex. If  $G_{max} = G = 2$  means that at  $\theta$  and  $\phi$  for which  $G$  is maximum, the power density of the source is twice that of the isotropic antenna



Ex:

A gsm base station antenna radiates E.M. waves with 10-100W of total output power. Evaluate the power density of the waves at  $R=100m$  away from the antenna in the broadside direction where the antenna has 12-18 dB for BTS and 2-5 dB for MS.

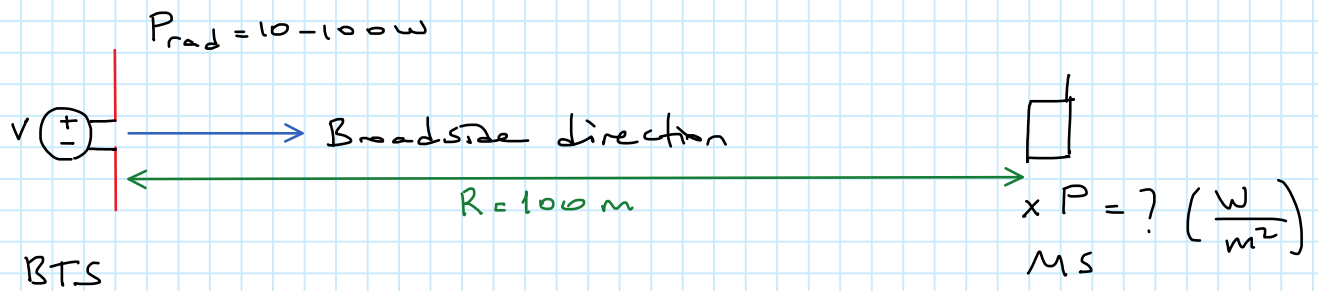
Base transceiver station

Mobile station.

Use  $G_{BTS} = 12 \text{ dB}$

Note All the given values are typized.

Ans



$$P = P_{iso} \cdot G(\theta = \frac{\pi}{2}) = \frac{P_{rad}}{4\pi R^2} \cdot G(\theta = \frac{\pi}{2})$$

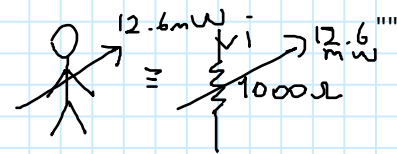
where

$$G(\theta = \frac{\pi}{2}) = 12 \text{ dB} = 10 \log \frac{G}{G_{ref}}, \quad G_{ref} = 1$$

$$12 = 10 \log G \Rightarrow G = 10^{1.2}$$

$$\Rightarrow P = \frac{10}{4\pi(100)^2} \cdot 10^{1.2} = 12.6 \frac{\text{mW}}{\text{m}^2}$$

$$P = \frac{100}{4\pi(100)^2} \cdot 10^{1.2} = 12.6 \frac{\text{mW}}{\text{m}^2}$$

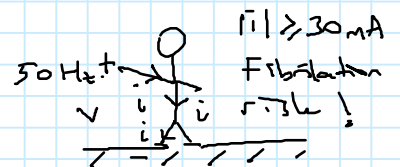


$$P_{avg} = \frac{1}{2} |i_i|^2 R$$

$$12.6 \text{ mW} = \frac{1}{2} \cdot |i_i|^2 \cdot 1000$$

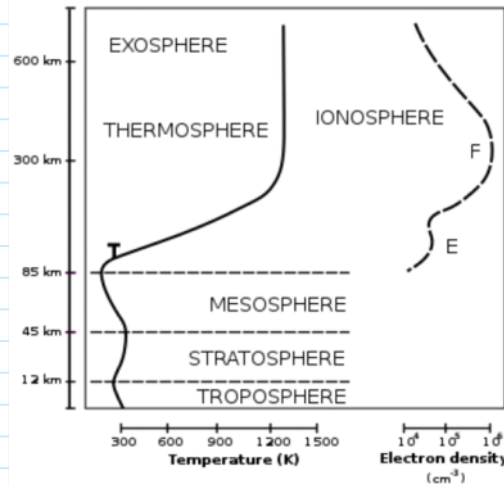
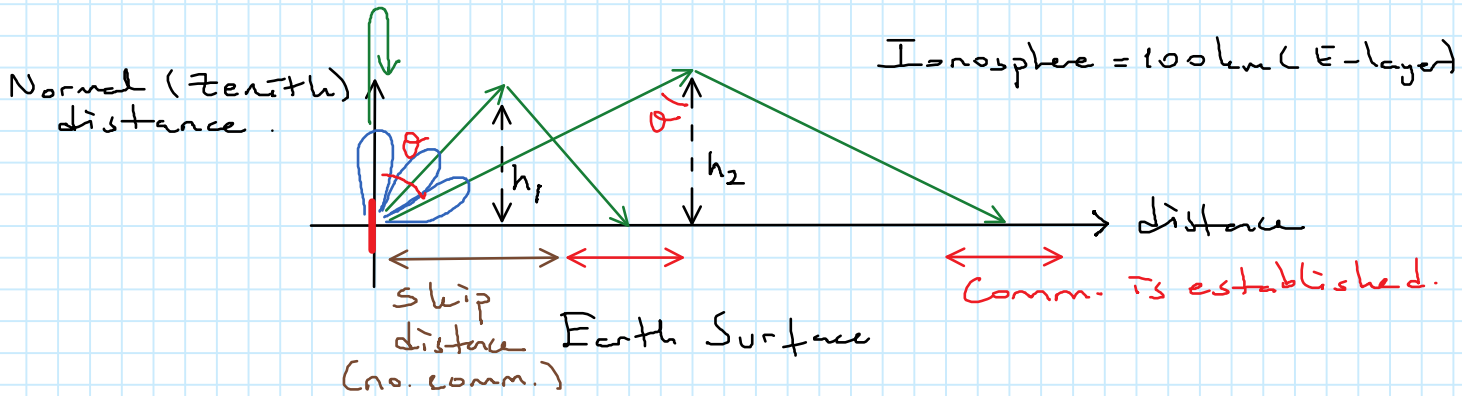
$$\frac{2 \cdot 12.6 \text{ mW}}{1000} = |i_i|^2$$

$$\Rightarrow |i_i| = 1.54 \text{ mA}$$



## 2-) Sky-Wave Propagation:

As waves travel through the ionosphere, they may reflect from a height  $h$ , and come back to the earth's surface at a distance  $d$  from the transmitter



### Maximum Usable Frequency (MUF):

Any E.M wave whose frequency below MUF reflects from the ionosphere from a height  $h$ . Waves with frequency above MUF escape to space.

- There is also the lowest usable frequency (LUF), and optimum working frequency (OWF).

By definition:

$$MUF = \frac{CF}{\cos \theta}$$

where  $CF$  = Critical frequency : Max freq for reflection at Zenith.  
 $\theta$  = Angle of incidence.

# P47

Monday, May 31, 2021 2:56 PM

It is given that

$$\text{OWF} = (0.85) \text{MUF}$$

(Best freq for skywave comm.)

Also,

$$CF = 9 \sqrt{N_{\max}}$$

where

$N_{\max}$  = Maximum  $e^-$  density

Generally,

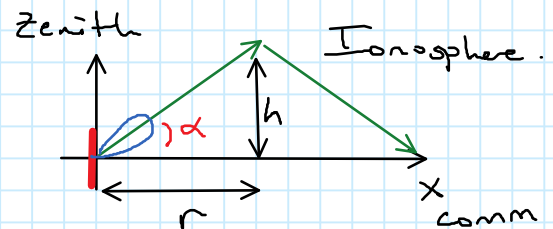
- Frequencies below 10MHz propagate most efficiently by skywaves at night
- Frequencies above 10MHz propagate most efficiently during the day
- At night, skip distance is increased.
- In VHF (30-300MHz), the skywave comm is not possible.
- Usually, HF (High Frequency  $\rightarrow$  3-30MHz) is used for sky wave comm.
- In attempt to calculate the radiation distance of the lowest angle beam (take-off angle), we can use the equation:

$$\tan \alpha = \frac{h}{r}$$

or

$$r = \frac{h}{\tan \alpha}$$

and the comm. distance =  $2r = \frac{2h}{\tan \alpha}$ , where  $\alpha = 90^\circ - \theta$



X Ex:

Given that the maximum  $e^-$  density in the ionosphere is  $N = 5 \times 10^4 \frac{e^-}{cm^3}$  and  $\theta = 70^\circ$ . Find the MUF and OMF.

Ans.

$$N_{max} = 5 \times 10^4 e^- \cdot cm^{-3} = 5 \times 10^{10} e^- \cdot m^{-3}$$

$$\Rightarrow CF = 9 \sqrt{N_{max}} = 9 \sqrt{5 \times 10^{10}} = 2 \times 10^6 \text{ Hz} = 2 \text{ MHz}$$

$$\Rightarrow MUF = \frac{CF}{\cos \theta} = \frac{2 \times 10^6}{\cos 70^\circ} = 5.884 \text{ MHz} \approx 6 \text{ MHz}$$

$$OMF = 0.85 MUF = 5 \text{ MHz}$$

- As a rule of thumb, MUF is about 3 times of CF.

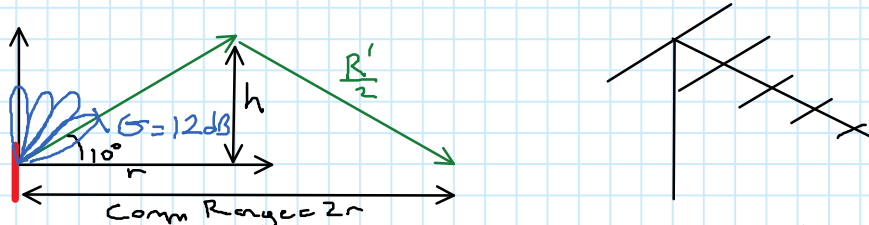
At  $\theta = 30^\circ$

$$MUF = \frac{2 \times 10^6}{\cos 30^\circ} = 2.3 \text{ MHz}$$

-  $MUF \propto \theta$  (Angle of incidence)

Ex.

For a horizontal polarized log-periodic dipole antenna with 1kW of radiated power, has the following radiation pattern:



Evaluate the maximum comm range through sky waves at a single hop of the smallest angle beam, and evaluate the power density at this distance. ( $h = 100 \text{ km} \rightarrow E\text{-layer}$ )

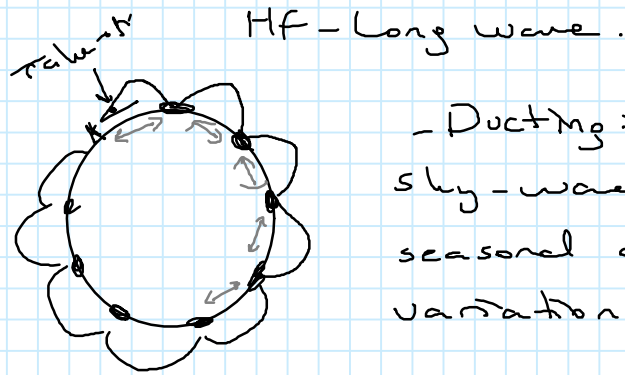
Ans.

$$\text{Range} = \frac{2h}{\tan \alpha} = \frac{2(10^5)}{\tan 10^\circ} = \frac{200000}{0.17} = 1176.47 \text{ km}$$

$$P = P_{iss} \cdot \text{Gain} = P_i \cdot G = \frac{P_{rad} \cdot G}{4\pi R^2} = \frac{1000 (10^{1.2})}{4\pi R^2} = \frac{1000 (10^{1.2})}{4\pi (1184000)^2}$$

$$\cos \alpha = \frac{r}{\frac{R'}{2}} \Rightarrow R' = \frac{1176.4 \text{ km}}{\cos 10^\circ} = \frac{1176.4 \text{ km}}{\cos 10^\circ} = 1194 \text{ km} \Rightarrow P = 8.85 \times 10^{-10} = 885 \frac{\text{pW}}{\text{m}^2}$$

↗ range of the wave propagation =  $R'$



- Ducting = Changes in sky-wave comm. due to seasonal and atmospheric variations

3-) Ground Wave Propagation:

The electric field expression for a ground wave -

$$E = E_0 e^{-\alpha z} e^{-j\beta z} \left(\frac{V}{m}\right)$$

or  $E(t, z) = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \left(\frac{V}{m}\right)$   $c = \frac{1}{\sqrt{\mu\epsilon}}$

where  $\alpha$  = Attenuation constant

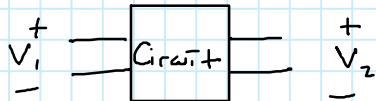
$\beta$  = Phase constant.  $\left(\beta = \omega\sqrt{\mu\epsilon} = 2\pi f\sqrt{\mu\epsilon} = \frac{2\pi f}{c} = \frac{2\pi}{\lambda}\right)$   
 $\left(\frac{1}{m}\right)$

Unit of  $\alpha$  = ?

The unit of  $\alpha$  is Nepers

Neper -

By definition, the voltage gain of the following circuit is



$$G_v = \frac{V_2}{V_1}$$

or in nepers -

$$G_{vNp} = \ln \frac{V_2}{V_1} = \ln V_2 - \ln V_1$$

Conversion from dB to Neper:

$$G_{dB} = 10 \log_{10} \frac{P_2}{P_1} = 10 \log_{10} \left(\frac{V_2}{V_1}\right)^2 = 20 \log_{10} \left(\frac{V_2}{V_1}\right)$$

Also,

$$G_{Np} = \ln \frac{V_2}{V_1} = \frac{\log_{10} \frac{V_2}{V_1}}{\log_{10} e} = \frac{G_{dB}}{20 \log_{10} e}$$

$$\Rightarrow \frac{G_{dB}}{G_{Np}} = 20 \log_{10} e \text{ where } e = 2.71828 \dots$$

$$= 8.68589 \frac{dB}{Np}$$

or

$$\frac{G_{Np}}{G_{dB}} = 0.11513 \frac{Np}{dB}$$

### Neper Analysis

$$G_{Np} = \ln \frac{U_2}{U_1} (Np)$$

Let us call  $\frac{U_2}{U_1} = m$ .

Then,

$$G_U = \ln m$$

or

$$m = e^{G_U}$$

$G_U$  is in Np.

Since for a ground wave,

$$E = E_0 e^{-\alpha z} e^{-j\beta z} \left( \frac{V}{m} \right)$$

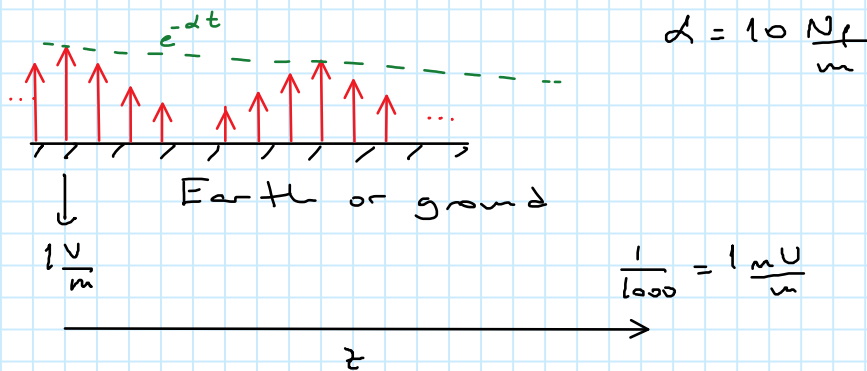
where  $\alpha z = Np$  Attenuation term

$$\Rightarrow \alpha = \frac{Np}{m} \text{ (attenuation constant)}$$

### Ex.

A vertical polarized dipole antenna radiates ground waves. The attenuation is  $10^{-3}$  Np/m. Find the distance at which the amplitude drops to 1000 of its original value!

### Ans.

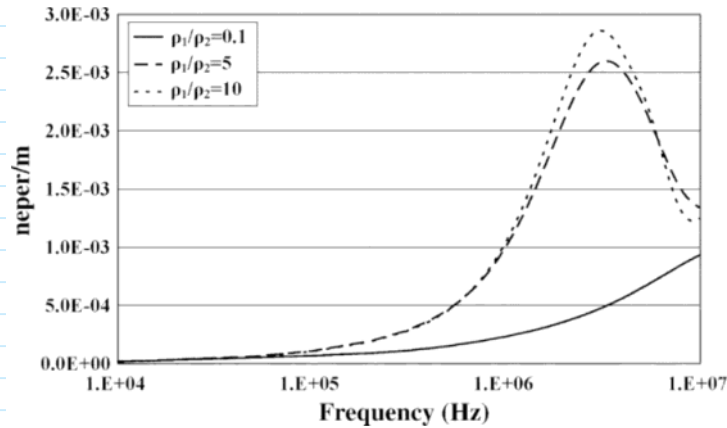


$$\alpha = 10 \frac{Np}{m}$$

$$\frac{E}{E_0} e^{-\alpha z} = \frac{1}{1000}$$

$$e^{-10^{-3} z} = \frac{1}{1000}$$

$$e^{10^{-3} z} = 1000 \Rightarrow 10^{-3} z = \ln 1000 \Rightarrow z = 6.9 \text{ km.}$$



TY - JOUR  
 AU - Papadopoulos, Theofilos  
 AU - Papagiannis, Grigoris  
 AU - Labridis, Dimitris  
 PY - 2009/03/01  
 SP - 1064  
 EP - 1067  
 T1 - Wave Propagation Characteristics of Overhead Conductors Above Imperfect Stratified Earth for a Wide Frequency Range  
 VL - 45  
 DO - 10.1109/TMAG.2009.2012580  
 JO - Magnetics, IEEE Transactions on ER